

3 Laminar Internal Flows - 114 to 120

1. Show that the axial velocity profile in a fully developed flow in an annulus is given by

$$\frac{u}{\bar{u}} = \frac{2}{A} \left[1 - \left(\frac{r}{r_o}\right)^2 + B \ln\left(\frac{r}{r_o}\right) \right]$$

where $B = ((r^*)^2 - 1)/\ln r^*$, $A = 1 + (r^*)^2 - B$ and $r^* = r_i/r_o$. Hence show that the maximum velocity will occur at $(r_m^*)^2 = 0.5B$ and $fRe = 16(1 - (r^*)^2)/A$

2. Determine Fully-Developed Pressure drop per unit length (N / m³) of the following ducts. In each case $Re_{D_{th}} = 500$. Take $\rho = 1000$ kg / m³, $\mu = 8 \times 10^{-4}$ kg/m-s. (Hint: Wherever possible, use solns given in the class. Else, evaluate from series solutions.)

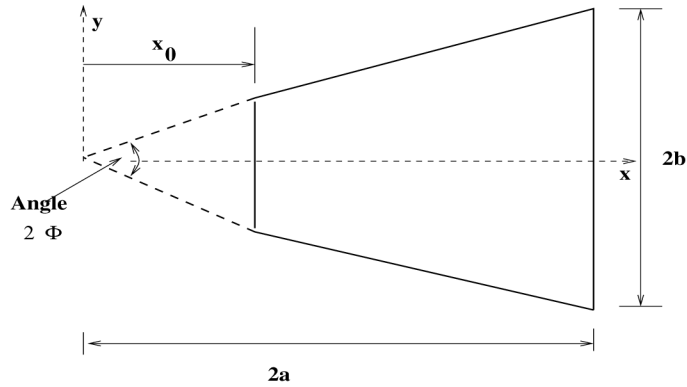


Figure 5: Duct of Rhombic cross-section

- (a) Rectangular duct: ($b = 1$ cm, $a = 4$ cm)
 - (b) Annulus ($r_i = 1$ cm, $r_o = 2.2$ cm)
 - (c) Annular Sector Duct ($r_i = 1$ cm, $r_o = 2.2$ cm, $\theta_0 = 60$ degrees)
 - (d) Equilateral Triangle: ($a = 2$ cm)
 - (e) Equilateral Triangle with Rounded Radius: ($a = 2$ cm, $r / a = 0.1$)
3. Using Kantarovich method, derive analytic expression for $(f Re)_{D_h} = F(x_0, b/a, \Phi)$ for the duct shown in figure 5.
 4. Write a general computer program for predicting $(f Re)_{D_h}$ and Nu_{D_h} in ducts of arbitrary cross section using the method described in lectures 16 and 18.
 5. Using the computer program developed in the previous problem, calculate $(f Re)_{D_h}$ and Nu_{D_h} for the duct shown in figure 5.
 6. Consider FD flow and heat transfer between two parallel plates. Include effect of viscous dissipation. Constant wall heat flux q_w is applied at both surfaces. Show that $(f Re)_{D_h} = 24$ and

$$Nu_{D_h} = \frac{140}{17 + 108 Br} \quad \text{where} \quad Br \equiv \frac{\mu \bar{u}^2}{q_w D_h}$$

7. A heat exchanger is to be designed to cool lubricating oil ($\rho = 785 \text{ kg/m}^3$, $k = 0.12 \text{ W / m-K}$, $\nu = 0.0247 \text{ m}^2/\text{hr}$ and $C_p = 2 \text{ kJ / kg - K}$) from 60 C to 40 C. The oil velocity is 0.75 m / s and the tube surface temperature is 27 C. Calculate the required tube (dia 6 mm) length.
8. Water at 35 C enters a tube (2.5 cm ID) with a velocity 1.25 m/s. The tube wall temperature is constant at 95 C. Calculate the tube-length necessary to raise water temperature by 45 C. Also calculate pumping power. Use a) Dittus-Boelter correlation b) Expression for Nu derived from universal law.
9. Liquid mercury flows through a long tube (2.5 cm dia) with a velocity 1 m/s. Calculate h for constant wall heat flux ($\rho = 13264 \text{ kg / m}^3$, $C_p = 0.1365 \text{ kJ/kg-K}$, $k = 11.5 \text{ W/m-K}$, $\mu = 9 \times 10^{-4} \text{ N-s/m}^2$)
10. Consider flow of air ($Pr = 0.7$) between two parallel plates 1 m wide and 2.5 cm apart. The top plate receives heat flux $q_{top} = 650 \text{ W/m}^2$ whereas the bottom plate is insulated. If $Re_{D_h} = 500$ and air enters the passage with $T_{in} = 32^\circ\text{C}$, calculate and plot variations of $T_{w,top}$ and $T_{w,bottom}$ till $x^+ = 0.1$ (Hint: Use results of slide 4, 119).
11. Consider flow of air in a passage formed by two parallel plates $W = 1$ m wide, $L = 1.4$ m long and separated by distance 3 mm. Heat flux at both the plates varies as

$$q_w = 950 + 2500 \sin\left(\frac{\pi x}{L}\right) \quad \left(\frac{W}{m^2}\right)$$

The air inlet temperature is 50°C and system pressure is 7 bar. If the air mass flux is $250 \text{ kg/m}^2\text{-hr}$, calculate and plot variation of T_b , T_w and Nu_x with axial distance x (m). Evaluate properties at 100°C .