

Stochastic Structural Dynamics

Lecture-15

Random vibration analysis of MDOF systems-3

Dr C S Manohar

Department of Civil Engineering
Professor of Structural Engineering
Indian Institute of Science
Bangalore 560 012 India
manohar@civil.iisc.ernet.in



Recall

$$\bullet [H(\omega)] = [-\omega^2 M + i\omega C + k]^{-1} = \left[\sum_{n=1}^N \frac{\Phi_{rn} \Phi_{sn}}{(\omega_n^2 - \omega^2 + i2\eta_n \omega_n \omega)} \right]$$

$$\bullet [h(t)] = [h_{rs}(t)] = \left[\sum_{n=1}^N \Phi_{rn} \Phi_{sn} \frac{1}{\omega_{dn}} \exp(-\eta_n \omega_n t) \sin \omega_{dn} t \right]$$

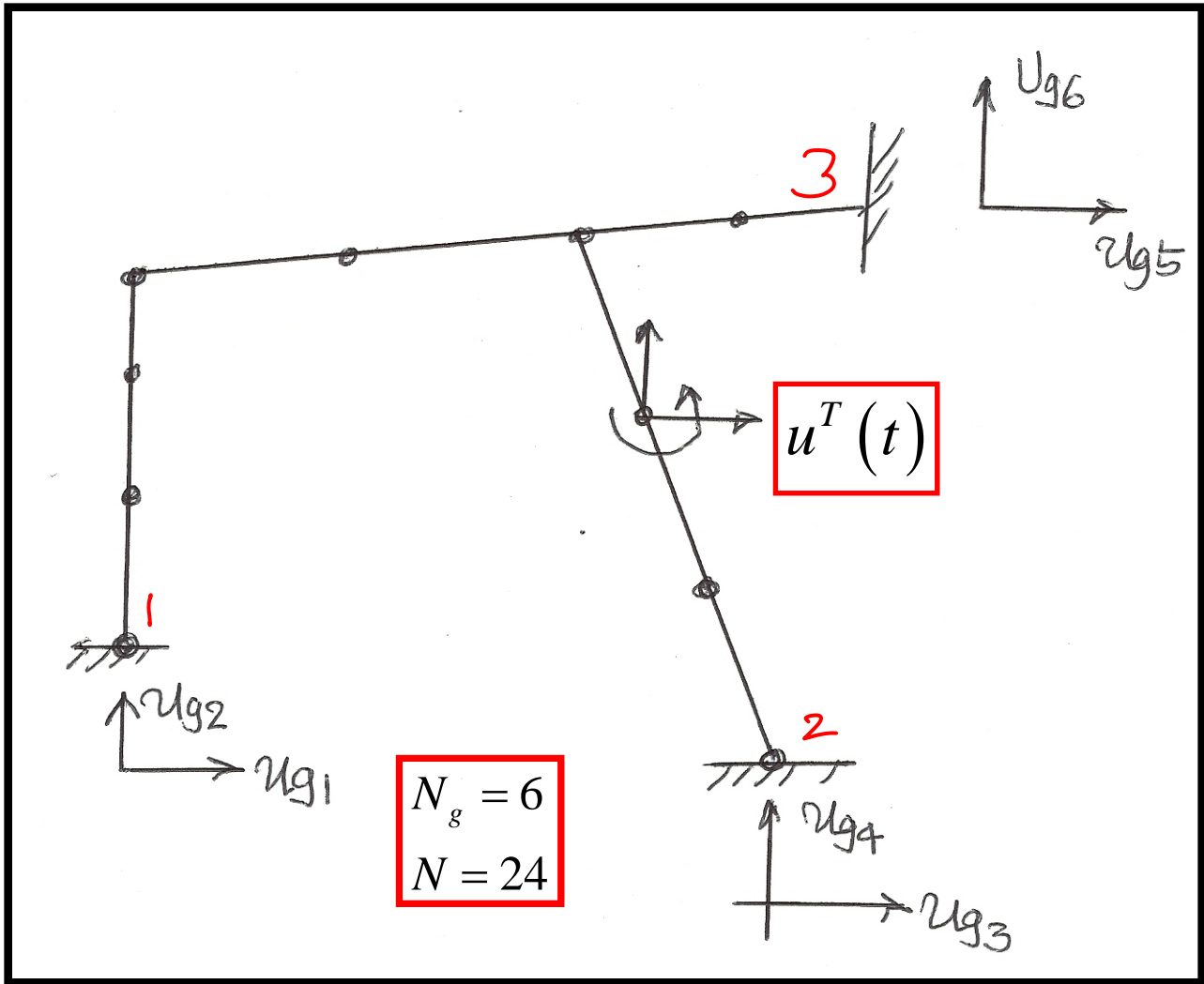
$$H_{ij}(\omega) = \int_{-\infty}^{\infty} h_{ij}(t) \exp(i\omega t) d\tau$$

$$h_{ij}(t) = \frac{1}{2\pi} \int_{-\infty}^{\infty} H_{ij}(\omega) \exp(-i\omega t) d\omega$$

$$S_{XX}(\omega) = H(\omega) S_{FF}(\omega) H^{*t}(\omega)$$

$$R_{XX}(t_1, t_2) = \int_0^{t_1} \int_0^{t_2} [h(t_1 - \tau_1)] R_{FF}(\tau_2 - \tau_1) [h(t_2 - \tau_2)]^t d\tau_1 d\tau_2$$

Structures under differential support motions



$$\begin{bmatrix} M & M_g \\ M_g^t & M_{gg} \end{bmatrix} \begin{Bmatrix} \ddot{u}^T \\ \ddot{u}_g \end{Bmatrix} + \begin{bmatrix} C & C_g \\ C_g^t & C_{gg} \end{bmatrix} \begin{Bmatrix} \dot{u}^T \\ \dot{u}_g \end{Bmatrix} + \begin{bmatrix} K & K_g \\ K_g^t & K_{gg} \end{bmatrix} \begin{Bmatrix} u^T \\ u_g \end{Bmatrix} = \begin{Bmatrix} 0 \\ p_g(t) \end{Bmatrix}$$

$$\ddot{u}^T \sim N \times 1$$

$$\ddot{u}_g, p_g(t) \sim N_g \times 1; N_T = N + N_g$$

$$M, C, K \sim N \times N$$

$$M_g, C_g, K_g \sim N \times N_g$$

$$M_{gg}, C_{gg}, K_{gg} \sim N_g \times N_g$$

Pseudo-dynamic response

$$\begin{bmatrix} K & K_g \\ K_g^t & K_{gg} \end{bmatrix} \begin{Bmatrix} u^p \\ u_g \end{Bmatrix} = \begin{Bmatrix} 0 \\ p_g^p(t) \end{Bmatrix}$$

$$Ku^p + K_g u_g = 0 \Rightarrow u^p = -K^{-1} K_g u_g(t) = \Gamma u_g(t)$$

$$\Gamma = -K^{-1} K_g$$

$$p_g^p(t) = K_g^t u^p + K_{gg} u_g = \left[-K_g^t K^{-1} K_g + K_{gg} \right] u_g(t)$$

Total response= pseudo-dynamic response + dynamic response

$$\begin{Bmatrix} u^T \\ u_g \end{Bmatrix} = \begin{Bmatrix} u^p(t) \\ u_g(t) \end{Bmatrix} + \begin{Bmatrix} u(t) \\ 0 \end{Bmatrix}$$

$$\begin{bmatrix} M & M_g \\ M_g^t & M_{gg} \end{bmatrix} \begin{Bmatrix} \ddot{u} + \ddot{u}^p(t) \\ \ddot{u}_g \end{Bmatrix} + \begin{bmatrix} C & C_g \\ C_g^t & C_{gg} \end{bmatrix} \begin{Bmatrix} \dot{u} + \dot{u}^p \\ \dot{u}_g \end{Bmatrix} +$$

$$\begin{bmatrix} K & K_g \\ K_g^t & K_{gg} \end{bmatrix} \begin{Bmatrix} u + u^p \\ u_g \end{Bmatrix} = \begin{Bmatrix} 0 \\ p_g(t) \end{Bmatrix}$$

\Rightarrow

$$M\ddot{u} + C\dot{u} + Ku = p_{eff}(t)$$

$$p_{eff}(t) = -M\ddot{u}^p(t) - M_g\ddot{u}_g - C\dot{u}^p(t) - C_g\dot{u}_g$$

$$= -M\Gamma\ddot{u}_g(t) - M_g\ddot{u}_g - \Gamma C\dot{u}_g(t) - C_g\dot{u}_g$$

$$= -[M\Gamma + M_g]\ddot{u}_g(t) - [C\Gamma + C_g]\dot{u}_g(t)$$

$$M\ddot{u} + C\dot{u} + Ku = -[M\Gamma + M_g]\ddot{u}_g(t) - [C\Gamma + C_g]\dot{u}_g(t)$$

Special Case

Mass matrix is diagonal $\Rightarrow M_g = 0$

C is proportional to K ($C = \alpha K$)

$$\Rightarrow [C\Gamma + C_g] = \alpha [K\Gamma + K_g] = \alpha [-KK^{-1}K_g + K_g] = 0$$

\Rightarrow

$$M\ddot{u} + C\dot{u} + Ku = -M\Gamma\ddot{u}_g(t)$$

$$\Gamma \sim N \times N_g$$

$$\ddot{u}_g(t) \sim N_g \times 1$$

Note: If all supports suffer the same motion, $N_g = 1$

$$\Gamma = \{1 \quad 1 \quad \dots \quad 1\}^t$$

Random vibration analysis in frequency domain

$$M\ddot{u} + C\dot{u} + Ku = -[M\Gamma + M_g]\ddot{u}_g(t) - [C\Gamma + C_g]\dot{u}_g(t) = p(t)$$

$u_g(t) \sim N_g \times 1$: vector of stationary random process with zero mean and PSD matrix

$$S_{gg}(\omega) = \lim_{T \rightarrow \infty} \frac{1}{T} \langle U_{gT}(\omega) U_{gT}^{*t}(\omega) \rangle$$

$$p(t) = -[M\Gamma + M_g]\ddot{u}_g(t) - [C\Gamma + C_g]\dot{u}_g(t)$$

$$P_T(\omega) = \omega^2 [M\Gamma + M_g] U_{gT}(\omega) - i\omega [C\Gamma + C_g] U_{gT}(\omega)$$

$$= \left[\omega^2 [M\Gamma + M_g] - i\omega [C\Gamma + C_g] \right] U_{gT}(\omega)$$

$$P_T^{*t}(\omega) = U_{gT}^{*t}(\omega) \left[\omega^2 [\Gamma^t M + M_g] + i\omega [\Gamma^t C + C_g] \right]$$

$$S_{pp}(\omega) = \lim_{T \rightarrow \infty} \frac{1}{T} \langle \left[\omega^2 [M\Gamma + M_g] - i\omega [C\Gamma + C_g] \right] U_{gT}(\omega)$$

$$U_{gT}^{*t}(\omega) \left[\omega^2 [\Gamma^t M + M_g] + i\omega [\Gamma^t C + C_g] \right] \rangle$$

$$S_{pp}(\omega) = \left[\omega^2 [M\Gamma + M_g] - i\omega [C\Gamma + C_g] \right]$$

$$S_{gg}(\omega) \left[\omega^2 [\Gamma^t M + M_g] + i\omega [\Gamma^t C + C_g] \right]$$

\Rightarrow

$$S_{UU}(\omega) = H(\omega) S_{pp}(\omega) H^{*t}(\omega)$$

$$\left[H(\omega) \right] = \left[-\omega^2 M + i\omega C + k \right]^{-1} = \left[\sum_{n=1}^N \frac{\Phi_{rn} \Phi_{sn}}{\left(\omega_n^2 - \omega^2 + i2\eta_n \omega_n \omega \right)} \right]$$

Pseudo-dynamic response

$$u^p = -K^{-1}K_g u_g(t) = \Gamma u_g(t)$$

$$\Gamma = -K^{-1}K_g$$

$$S_{u^p u^p}(\omega) = \Gamma S_{g g}(\omega) \Gamma^t$$

Total response

$$u^T(t) = u^p(t) + u(t)$$

$$= \Gamma u_g(t) + u(t)$$

$$U_T^T(\omega) = \Gamma U_{gT}(\omega) + U_T(\omega)$$

$$= \Gamma U_{gT}(\omega) + H(\omega) P_T(\omega)$$

$$P_T(\omega) = \left[\omega^2 [M\Gamma + M_g] - i\omega [C\Gamma + C_g] \right] U_{gT}(\omega)$$

\Rightarrow

$$U_T^T(\omega) = \left[\Gamma + \omega^2 [M\Gamma + M_g] - i\omega [C\Gamma + C_g] \right] U_{gT}(\omega)$$

Total response

$$U_T^T(\omega) = \left[\Gamma + \omega^2 [M\Gamma + M_g] - i\omega [C\Gamma + C_g] \right] U_{gT}(\omega)$$

\Rightarrow

$$S_{TT}(\omega) = \left[\Gamma + \omega^2 [M\Gamma + M_g] - i\omega [C\Gamma + C_g] \right] S_{gg}(\omega)$$

$$\left[\Gamma + \omega^2 [M\Gamma + M_g] - i\omega [C\Gamma + C_g] \right]^t$$

Variance of total response=

variance of pseudo-dynamic response+

variance of dynamic response+

contributions due to correlation between

pseudo-dynamic and dynamic responses

Random vibration analysis in time domain

$$M\ddot{u} + C\dot{u} + Ku = -[M\Gamma + M_g]\ddot{u}_g(t) - [C\Gamma + C_g]\dot{u}_g(t) = p(t)$$

$u_g(t) \sim N_g \times 1$: vector of stationary random process with zero mean and auto-covariance matrix

$$R_{gg}(t_1, t_2) = \langle u_g(t_1)u_g^t(t_2) \rangle = R_{gg}(t_1 - t_2)$$

$$p(t_1) = -[M\Gamma + M_g]\ddot{u}_g(t_1) - [C\Gamma + C_g]\dot{u}_g(t_1)$$

$$p^t(t_2) = -\ddot{u}_g^t(t_2)[\Gamma^t M + M_g] - \dot{u}_g^t(t_2)[\Gamma^t C + C_g]$$

$$\begin{aligned}
\langle p(t_1) p^t(t_2) \rangle &= R_{pp}(t_1, t_2) \\
&= [M\Gamma + M_g] \langle \ddot{u}_g(t_1) \ddot{u}_g^t(t_2) \rangle [\Gamma^t M + M_g] \\
&+ [M\Gamma + M_g] \langle \ddot{u}_g(t_1) \dot{u}_g^t(t_2) \rangle [\Gamma^t C + MC_g] \\
&+ [C\Gamma + C_g] \langle \dot{u}_g(t_1) \ddot{u}_g^t(t_2) \rangle [\Gamma^t M + M_g] \\
&+ [C\Gamma + C_g] \langle \dot{u}_g(t_1) \dot{u}_g^t(t_2) \rangle [\Gamma^t C + MC_g] \\
R_{UU}(t_1, t_2) &= \int_0^{t_1} \int_0^{t_2} [h(t_1 - \tau_1)] R_{pp}(\tau_2 - \tau_1) [h(t_2 - \tau_2)]^t d\tau_1 d\tau_2
\end{aligned}$$

$$[h(t)] = [h_{rs}(t)] = \left[\sum_{n=1}^N \Phi_{rn} \Phi_{sn} \frac{1}{\omega_{dn}} \exp(-\eta_n \omega_n t) \sin \omega_{dn} t \right]$$

Recall

$$\left\langle \frac{d^n X}{dt^n} \Big|_{t=t_1} \frac{d^m X}{dt^m} \Big|_{t=t_2} \right\rangle = \frac{\partial^{n+m} R_{XX}(t_1, t_2)}{\partial t_1^n \partial t_2^m}$$

$$\left\langle \frac{d^n X(t + \tau)}{dt^n} \frac{d^m Y(t)}{dt^m} \right\rangle = (-1)^m \frac{d^{n+m} R_{XY}(\tau)}{d\tau^{n+m}}$$

Total response= pseudo-dynamic response+dynamic response

$$u^T(t) = u^p(t) + u(t)$$

$$= \Gamma u_g(t) + u(t)$$

$$= \Gamma u_g(t) + \int_0^t [h(t-\tau)] \left\{ -[M\Gamma + M_g] \ddot{u}_g(\tau) - [C\Gamma + C_g] \dot{u}_g(\tau) \right\} d\tau$$

Variance of total response=

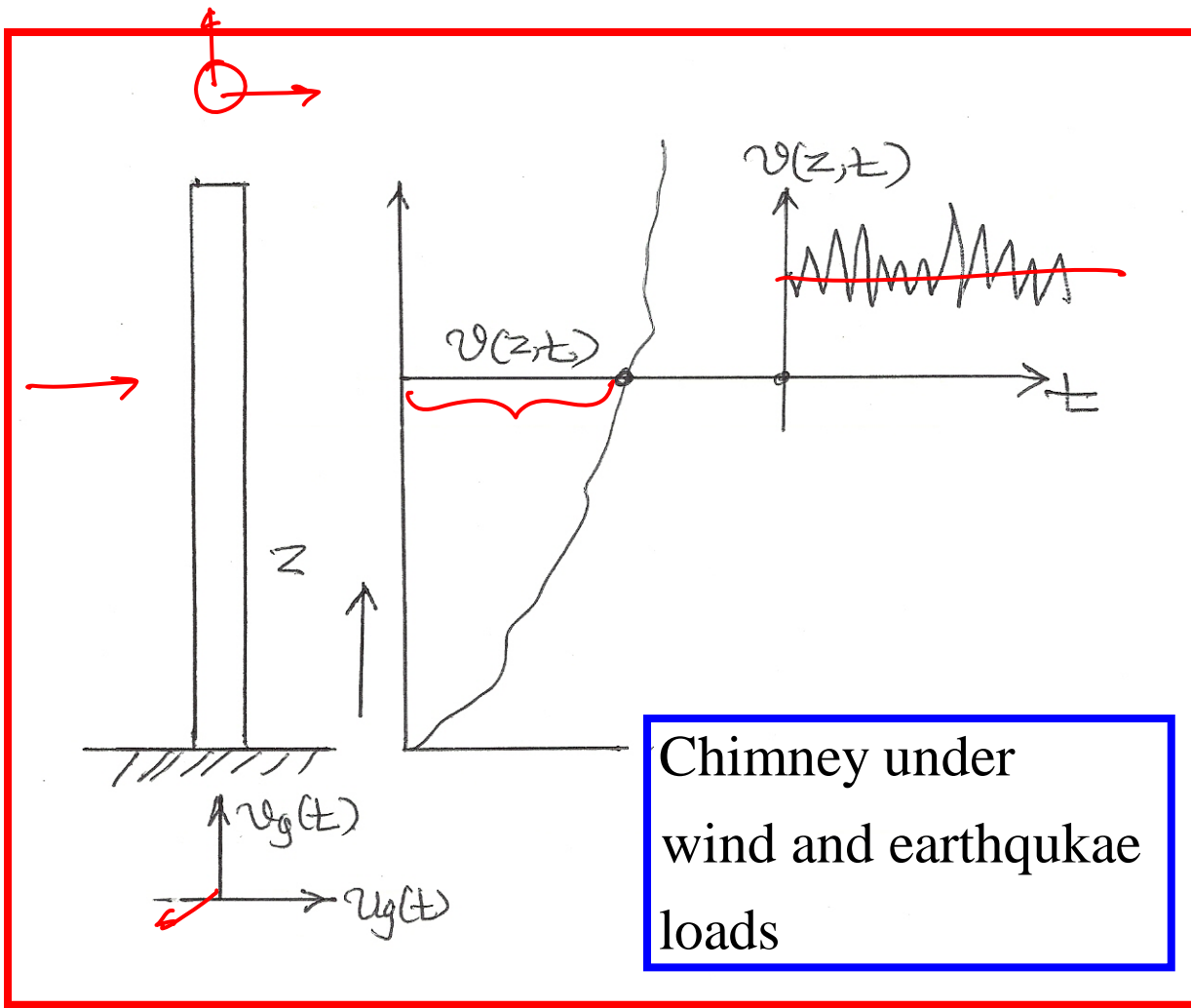
variance of pseudo-dynamic response+

variance of dynamic response+

contributions due to correlation between

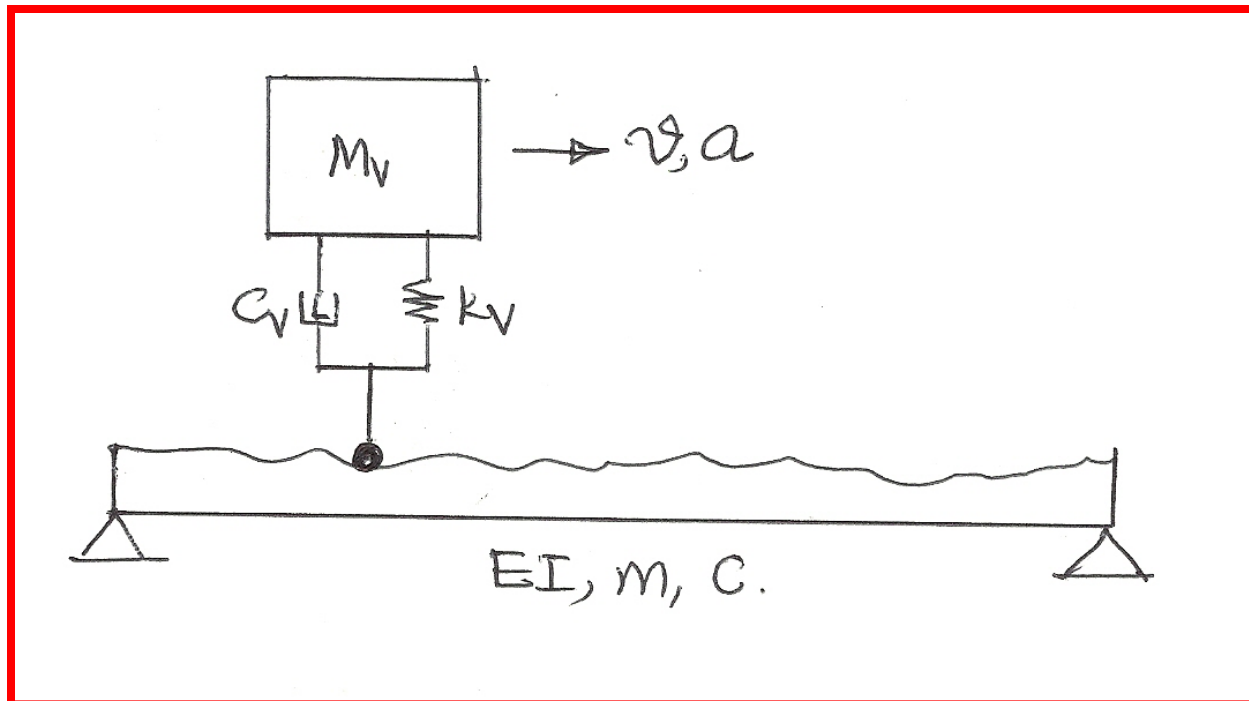
pseudo-dynamic and dynamic responses

RANDOM VIBRATION ANALYSIS OF CONTINUOUS MDOF SYSTEMS



Vehicle structure interaction

- Guideway unevenness
- Vehicle motion
- Vehicle parameters



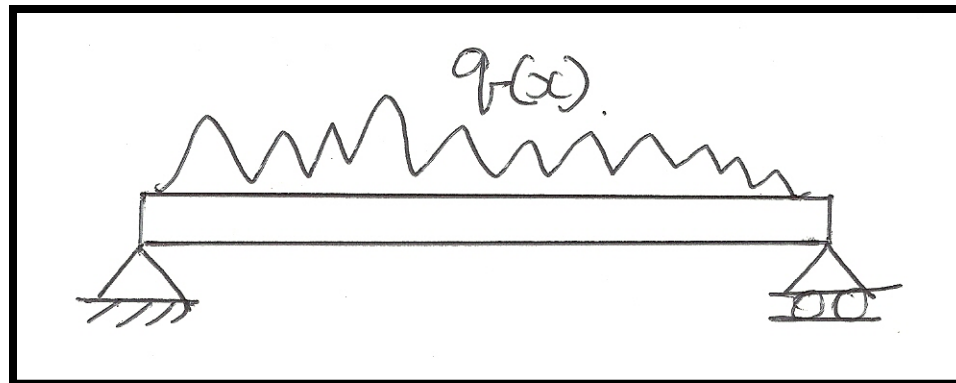
Re view of dynamics of Euler-Bernoulli beams
under deterministic excitations

Statically loaded beam

$$\frac{d^2}{dx^2} \left[EI(x) \frac{d^2 y}{dx^2} \right] = q(x)$$

$$y(0) = 0; y(l) = 0$$

$$y'(0) = 0; EI \frac{d^2 y}{dx^2} (l) = 0$$



Dynamically loaded beam

$$\frac{\partial^2}{\partial x^2} \left[EI(x) \frac{\partial^2 y}{\partial x^2} + \underline{a(x)} \frac{\partial^3 y}{\partial x^2 \partial t} \right] + \underline{m(x)} \frac{\partial^2 y}{\partial t^2} + \underline{c(x)} \frac{\partial y}{\partial t} = q(x, t)$$



Strain rate dependent
viscous damping

velocity dependent
viscous damping

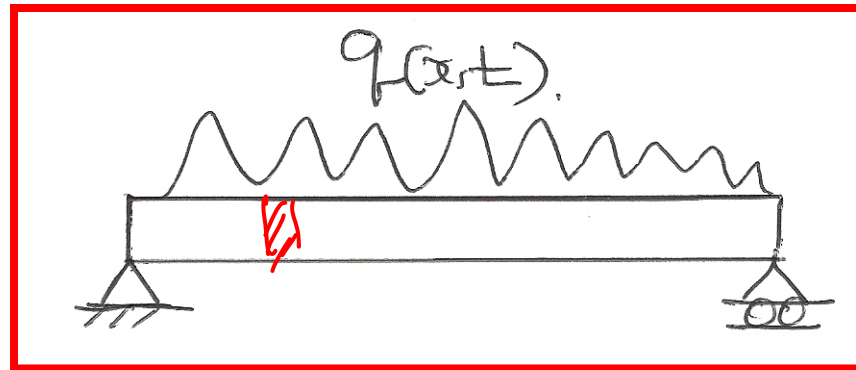
BCS

$$y(0, t) = 0; y(l, t) = 0$$

$$y'(0, t) = 0; EI \frac{\partial^2 y}{\partial x^2}(l, t) = 0$$

ICS

$$y(x, 0) = y_0(x); \frac{\partial y}{\partial t}(x, 0) = \dot{y}_0(x)$$



Undamped free vibration analysis

$$\frac{\partial^2}{\partial x^2} \left[EI(x) \frac{\partial^2 y}{\partial x^2} \right] + m(x) \frac{\partial^2 y}{\partial t^2} = 0$$

BCS

$$y(0, t) = 0; y(l, t) = 0$$

$$y'(0, t) = 0; EI \frac{\partial^2 y}{\partial x^2}(l, t) = 0$$

Seek the solution in the form

$$y(x, t) = \phi(x)T(t)$$

\Rightarrow

$$\left[EI\phi''(x) \right]'' T(t) + \phi(x)m(x)\ddot{T}(t) = 0$$

Note

$$(\quad)' = \frac{\partial}{\partial x} \quad \& \quad \ddot{T}(t) = \frac{\partial^2 T}{\partial t^2}$$

$$\left[EI\phi''(x) \right]'' T(t) + \phi(x)m(x)\ddot{T}(t) = 0$$

\Rightarrow

$$\frac{\left[EI\phi''(x) \right]'' T(t)}{\phi(x)T(t)} + \frac{\phi(x)m(x)\ddot{T}(t)}{\phi(x)T(t)} = 0$$

$$\frac{\left[EI\phi''(x) \right]''}{\phi(x)m(x)} = -\frac{\ddot{T}(t)}{T(t)} = \text{constant} = \omega^2$$

\Rightarrow

$$\ddot{T}(t) + \omega^2 T(t) = 0 \Rightarrow T(t) = A \cos(\omega t) + B \sin(\omega t)$$

$$\left[EI\phi''(x) \right]'' - \omega^2 m(x)\phi(x) = 0$$

$$y(0,t) = 0; y(l,t) = 0; y'(0,t) = 0; EI \frac{\partial^2 y}{\partial x^2}(l,t) = 0$$

$$\Rightarrow \phi(0) = 0; \phi(l) = 0; \phi'(0) = 0; EI \frac{d^2 \phi}{dx^2}(l) = 0$$

Eigenvalue problem

$$\left[EI(x) \phi''(x) \right]'' - \omega^2 m(x) \phi(x) = 0$$

$$\phi(0) = 0; \phi(l) = 0; \phi'(0) = 0; EI \frac{d^2 \phi}{dx^2}(l) = 0$$

$$\phi(x) = e^{sx}$$

Special case

$$EI(x) = EI; m(x) = m$$

$$EI \phi^{iv}(x) - \omega^2 m \phi(x) = 0$$

$$\lambda^4 = \frac{m\omega^2}{EI}$$

$$s^4 - \lambda^4 = 0$$

$$s = \pm \lambda, \pm i\lambda$$

$$\phi^{iv} - \lambda^4 \phi = 0$$

$$\phi(x) = a(\cos \lambda x + \cosh \lambda x) + b(\cos \lambda x - \cosh \lambda x)$$

$$+ c(\sin \lambda x + \sinh \lambda x) + d(\sin \lambda x - \sinh \lambda x)$$

$$\phi'(x) = a\lambda(-\sin \lambda x + \sinh \lambda x) + b\lambda(-\sin \lambda x - \sinh \lambda x)$$

$$+ c\lambda(\cos \lambda x + \cosh \lambda x) + d\lambda(\cos \lambda x - \cosh \lambda x)$$

$$\phi''(x) = a\lambda^2(-\cos \lambda x + \cosh \lambda x) + b\lambda^2(-\cos \lambda x - \cosh \lambda x)$$

$$+ c\lambda^2(-\sin \lambda x + \sinh \lambda x) + d\lambda^2(-\sin \lambda x - \sinh \lambda x)$$

$$\phi(0) = 0; \phi(l) = 0; \phi'(0) = 0; EI \frac{d^2\phi}{dx^2}(l) = 0$$

$$\phi(x) = a(\cos \lambda x + \cosh \lambda x) + b(\cos \lambda x - \cosh \lambda x)$$

$$+ c(\sin \lambda x + \sinh \lambda x) + d(\sin \lambda x - \sinh \lambda x)$$

$$\phi'(x) = a\lambda(-\sin \lambda x + \sinh \lambda x) + b\lambda(-\sin \lambda x - \sinh \lambda x)$$

$$+ c\lambda(\cos \lambda x + \cosh \lambda x) + d\lambda(\cos \lambda x - \cosh \lambda x)$$

$$\phi''(x) = a\lambda^2(-\cos \lambda x + \cosh \lambda x) + b\lambda^2(-\cos \lambda x - \cosh \lambda x)$$

$$+ c\lambda^2(-\sin \lambda x + \sinh \lambda x) + d\lambda^2(-\sin \lambda x - \sinh \lambda x)$$

$$\phi(0) = 0 \Rightarrow a = 0$$

$$\phi'(0) = 0 \Rightarrow c = 0$$

$$\phi(l) = 0 \Rightarrow b(\cos \lambda l - \cosh \lambda l) + d(\sin \lambda l - \sinh \lambda l)$$

$$\phi''(l) = 0 \Rightarrow b\lambda^2(-\cos \lambda l - \cosh \lambda l) + d\lambda^2(-\sin \lambda l - \sinh \lambda l)$$

$$\phi(l) = 0 \Rightarrow b(\cos \lambda l - \cosh \lambda l) + d(\sin \lambda l - \sinh \lambda l)$$

$$\phi''(l) = 0 \Rightarrow b\lambda^2(-\cos \lambda l - \cosh \lambda l) + d\lambda^2(-\sin \lambda l - \sinh \lambda l)$$

\Rightarrow

$$\begin{bmatrix} (\cos \lambda l - \cosh \lambda l) & (\sin \lambda l - \sinh \lambda l) \\ \lambda^2(-\cos \lambda l - \cosh \lambda l) & \lambda^2(-\sin \lambda l - \sinh \lambda l) \end{bmatrix} \begin{Bmatrix} b \\ d \end{Bmatrix} = 0$$

\Rightarrow

$$\begin{vmatrix} (\cos \lambda l - \cosh \lambda l) & (\sin \lambda l - \sinh \lambda l) \\ \lambda^2(-\cos \lambda l - \cosh \lambda l) & \lambda^2(-\sin \lambda l - \sinh \lambda l) \end{vmatrix} = 0$$

$$\Rightarrow \tan \lambda l = \tanh \lambda l \Rightarrow \{\lambda_n\}_{n=1}^{\infty} : \text{characteristic values}$$

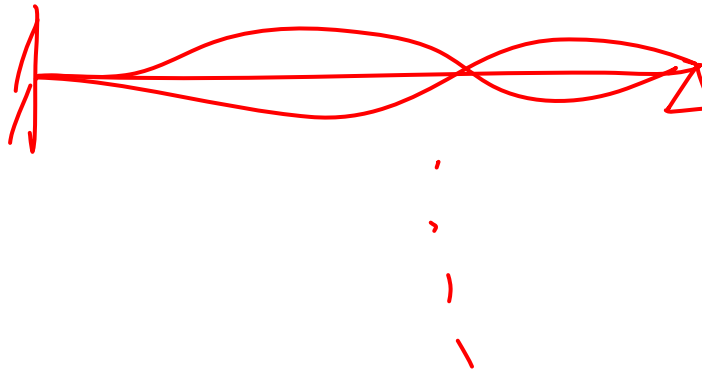
$$\phi_n(x) = (\cosh \lambda_n x - \cos \lambda_n x) + \underline{\underline{\sigma_n}} (\sinh \lambda_n x - \sin \lambda_n x) //$$

$$\sigma_n = \frac{\cos \lambda_n l - \cosh \lambda_n l}{\sin \lambda_n l - \sinh \lambda_n l} //$$


$$\omega_n = C_n \sqrt{\frac{EI}{ml^4}}; C_n = (\lambda_n l)^2$$

$$\{C_n\}_{n=1}^5 = 15.4118, 49.9648, 104.2477, 178.2697, 272.0309$$

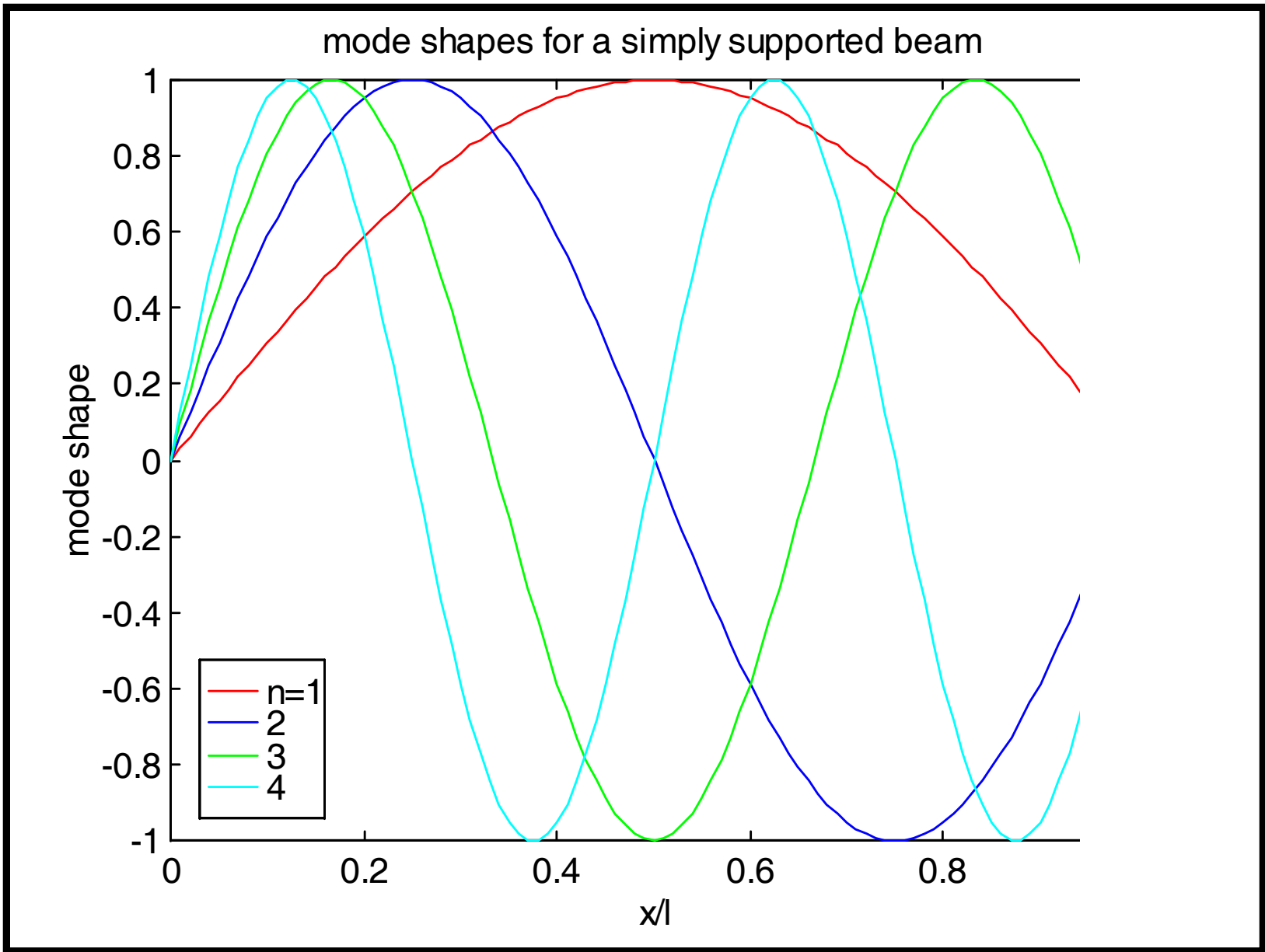
$$\{\sigma_n\}_{n=1}^5 = 1.000777, 1.000001, 1.000000, 1.000000, 1.000000$$



Homogeneous simply supported beam


$$\omega_n = \frac{n^2 \pi^2}{L^2} \sqrt{\frac{EI}{m}} \quad n = 1, 2, \dots, \infty$$
$$\varphi_n(x) = \sin \frac{n\pi x}{L}$$

Exercise



Orthogonality conditions

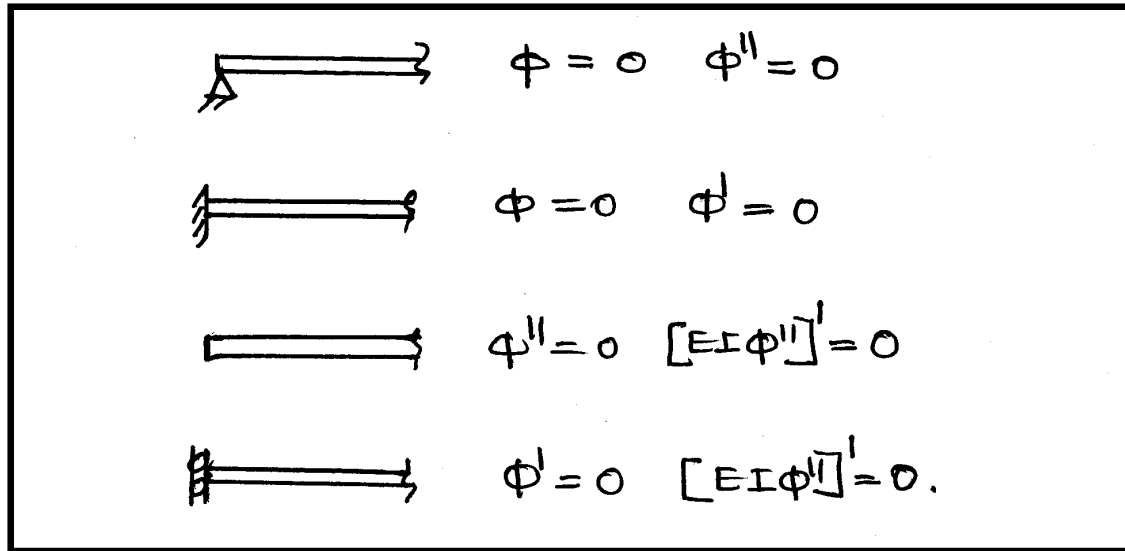
$$[EI\phi_n'']'' = m\omega_n^2 \phi_n \dots\dots (1) \leftarrow$$

$$[EI\phi_k'']'' = m\omega_k^2 \phi_k \dots\dots (2)$$

$$\int_0^L \phi_k [EI\phi_n'']'' dx = \int_0^L m\omega_n^2 \phi_k \phi_n dx \dots\dots (3)$$

$$\int_0^L \phi_n [EI\phi_k'']'' dx = \int_0^L m\omega_k^2 \phi_k \phi_n dx \dots\dots (4)$$

$$\begin{aligned}
\int_0^L \phi_n [EI \phi_k''] dx &= \underbrace{\left\{ \phi_k [EI \phi_k'] \right\}_0^L} - \int_0^L \phi_n' [EI \phi_k'] dx \\
&= \underbrace{\left\{ \phi_k [EI \phi_k'] \right\}_0^L}_0 - \underbrace{\left\{ \phi_n' [EI \phi_k'] \right\}_0^L}_0 + \int_0^L \phi_n'' EI \phi_k'' dx
\end{aligned}$$



$\Phi^t K \Phi$ being diagonal

$$\Rightarrow \int_0^L EI(x) \phi_n''(x) \phi_k''(x) dx = 0 \text{ for } n \neq k$$

$$\int_0^L m(x) \phi_n(x) \phi_k(x) dx = 0 \text{ for } n \neq k$$

Il y a $\Phi^t M \Phi$ diagonal

Forced response analysis using eigenfunction expansion

$$\frac{\partial^2}{\partial x^2} \left[EI(x) \frac{\partial^2 y}{\partial x^2} + \varepsilon(x) \frac{\partial^3 y}{\partial x^2 \partial t} \right] + m(x) \ddot{y} + c(x) \dot{y} = f(x, t)$$

ICS: $y_0(x) = y(x, 0)$ $\dot{y}_0(x) = \dot{y}(x, 0)$ & BCS as appropriate.

$$y(x, t) = \sum_{n=1}^{\infty} a_n(t) \varphi_n(x)$$

Known (pointing to $\varphi_n(x)$)
Unknowns (pointing to $a_n(t)$)
Gen-co-ordinates (pointing to $a_n(t)$)

$$[EI \varphi_n'']'' = m \omega_n^2 \varphi_n(x)$$

$$\int_0^L EI \varphi_n'' \varphi_k'' dx = 0 \quad n \neq k \quad \int_0^L m \varphi_n \varphi_k dx = 0 \quad n \neq k$$

$$[EI \sum_{n=1}^{\infty} a_n(t) \varphi_n'' + \varepsilon \sum_{n=1}^{\infty} \dot{a}_n(t) \varphi_n'']'' + c(x) \sum_{n=1}^{\infty} \dot{a}_n(t) \varphi_n + m(x) \sum_{n=1}^{\infty} \ddot{a}_n(t) \varphi_n = f(x, t)$$

$$\sum_{n=1}^{\infty} a_n(t) [EI \varphi_n'']'' + \sum_{n=1}^{\infty} \dot{a}_n(t) [\varepsilon(x) \varphi_n']'' + c(x) \sum_{n=1}^{\infty} \dot{a}_n(t) \varphi_n + m(x) \sum_{n=1}^{\infty} \ddot{a}_n(t) \varphi_n = f(x, t)$$

$$\sum_{n=1}^{\infty} a_n(t) m \omega_n^2 \varphi_n + \sum_{n=1}^{\infty} \dot{a}_n(t) [\varepsilon(x) \varphi_n']'' + c(x) \sum_{n=1}^{\infty} \dot{a}_n(t) \varphi_n + m(x) \sum_{n=1}^{\infty} \ddot{a}_n(t) \varphi_n = f(x, t)$$

Proportional damping model

$$C = \underline{\alpha M} + \beta K$$

$$\underline{\varepsilon(x)} = \underline{\nu EI(x)}$$

(Damping force proportional to time rate of bending strain)

$$c(x) = \underline{\alpha m(x)}$$

(Damping force is proportional to velocity)

$$\sum_{n=1}^{\infty} a_n(t) m \omega_n^2 \varphi_n + \nu \sum_{n=1}^{\infty} \dot{a}_n(t) \underbrace{[EI(x) \varphi_n'']'} + \underbrace{\alpha m(x)} \sum_{n=1}^{\infty} \dot{a}_n(t) \varphi_n + m(x) \sum_{n=1}^{\infty} \ddot{a}_n(t) \varphi_n = f(x, t)$$

$$\sum_{n=1}^{\infty} a_n(t) m \omega_n^2 \varphi_n + \nu \sum_{n=1}^{\infty} \dot{a}_n(t) \underbrace{m \omega_n^2 \varphi_n(x)} + \underbrace{\alpha m(x)} \sum_{n=1}^{\infty} \dot{a}_n(t) \varphi_n + m(x) \sum_{n=1}^{\infty} \ddot{a}_n(t) \varphi_n = f(x, t)$$

$$\sum_{n=1}^{\infty} a_n(t) \omega_n^2 \int_0^L m(x) \phi_k \phi_n dx + \nu \sum_{n=1}^{\infty} \dot{a}_n(t) \omega_n^2 \int_0^L m(x) \phi_k \phi_n dx$$

$$+ \sum_{n=1}^{\infty} \dot{a}_n(t) \int_0^L c(x) \phi_k \phi_n dx + \sum_{n=1}^{\infty} \ddot{a}_n(t) \int_0^L m(x) \phi_k \phi_n dx = \int_0^L \phi_k(x) f(x, t) dx$$

$$\Rightarrow m_n \ddot{a}_n + m_n (\alpha + v\omega_n^2) \dot{a}_n + m_n \omega_n^2 a_n = \bar{p}_n(t)$$

$$\Rightarrow \ddot{a}_n + (\alpha + v\omega_n^2) \dot{a}_n + \omega_n^2 a_n = \frac{\bar{p}_n(t)}{m_n} = p_n(t)$$

$n=1, 2, \dots, \infty$

$$m_n = \int_0^L m(x) \phi_n^2(x) dx$$

$$\ddot{a}_n + \underline{2\eta_n \omega_n} \dot{a}_n + \omega_n^2 a_n = p_n(t);$$

$$2\eta_n \omega_n = (\alpha + v\omega_n^2);$$

$$p_n(t) = \frac{\int_0^L \varphi_n(x) f(x, t) dx}{\int_0^L \varphi_n^2(x) m(x) dx} \quad n = 1, 2, \dots, \infty$$

Initial conditions

$$y(x, t) = \sum_{k=1}^{\infty} a_k(t) \phi_k(x)$$

$$\Rightarrow y(x, 0) = \sum_{k=1}^{\infty} a_k(0) \phi_k(x)$$

$$\Rightarrow \overset{m_n}{a_n}(0) = \int_0^L m(x) \phi_n(x) y(x, 0) dx \quad \overset{m_n}{\dot{a}_n}(0) = \int_0^L m(x) \phi_n(x) \dot{y}(x, 0) dx$$

Final solution

$$y(x,t) = \sum_{n=1}^{\infty} \phi_n(x) \left\{ \exp(-\eta_n \omega_n t) [A_n \cos \omega_{dn} t + B_n \sin \omega_{dn} t] + \int_0^t h_n(t-\tau) p_n(\tau) d\tau \right\}$$

$$\theta(x,t) = \frac{\partial y}{\partial x} \quad \text{BM} = EI \frac{\partial^2 y}{\partial x^2}$$

Remark:

$$\text{SF} = \frac{\partial}{\partial x} \left(EI \frac{\partial^2 y}{\partial x^2} \right)$$

Once the displacement field is found,
we can easily find stress resultants (BM and SF)
and the required bending/shear stresses

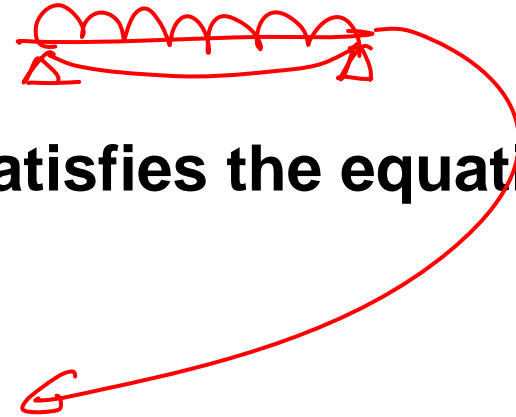
Example 1: An undamped simply supported beam carries an udl. The load is suddenly removed. Determine the ensuing vibrations.

Solution:

The initial deflection of the beam satisfies the equation

$$EIy_0^{iv} = q$$

Assume that the initial velocity of the beam is zero.



$$y(x, t) = \sum_{n=1}^{\infty} a_n(t) \varphi_n(x) \quad \ddot{a}_n + \omega_n^2 a_n = 0$$

$$\Rightarrow a_n(t) = A_n \cos \omega_n t + B_n \sin \omega_n t$$

$$\dot{y}(x, 0) = 0 \Rightarrow \dot{a}_n(0) = 0 \Rightarrow y(x, t) = \sum_{n=1}^{\infty} A_n \cos \omega_n t \sin \frac{n\pi x}{L}$$

$$\Rightarrow y(x, 0) = \sum_{n=1}^{\infty} A_n \sin \frac{n\pi x}{L} = y_0(x)$$

$$EI y_0^{iv} = q \Rightarrow \sum_{n=1}^{\infty} EI \left(\frac{n\pi}{L} \right)^4 A_n \sin \frac{n\pi x}{L} = q \Rightarrow A_n = \frac{4L^4}{n^5 \pi^5} \left(\frac{q}{EI} \right)$$

$$y(x, t) = \sum_{n=1,3,5,\dots}^{\infty} \frac{4L^4}{n^5 \pi^5} \left(\frac{q}{EI} \right) \cos \omega_n t \sin \frac{n\pi x}{L}$$

Example 2: An udl is suddenly applied on an undamped simply supported beam. Determine the ensuing vibrations. Assume that the beam is at rest at $t=0$.

$$EIy^{iv} + m\ddot{y} = \underline{qU(t)}$$

$$y(x,t) = \sum_{n=1}^{\infty} a_n(t) \sin \frac{n\pi x}{L}$$

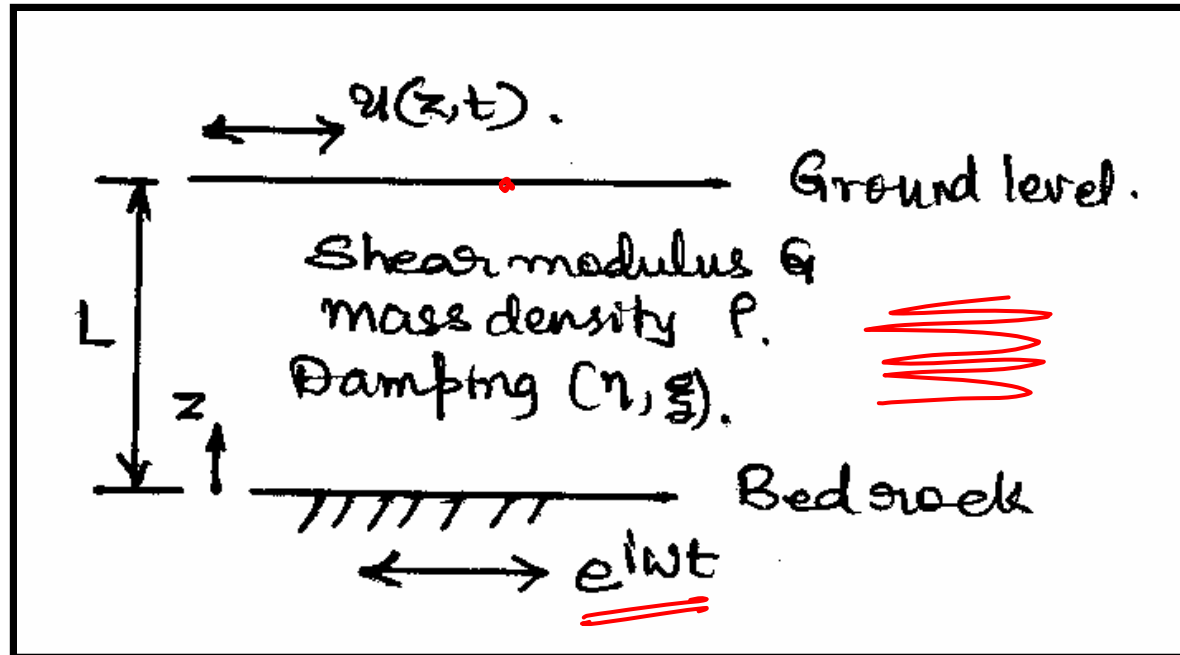
$$\ddot{a}_n + \omega_n^2 a_n = \frac{q}{m_n} \int_0^L U(t) q \sin \frac{n\pi x}{L} dx$$

EX



$$y(x,t) = \sum_{n=1,3,5,\dots}^{\infty} \frac{2qL}{n\pi m_n \omega_n^2} (1 - \cos \omega_n t) \sin \frac{n\pi x}{L}$$

Seismic wave amplification through soil layers



$$\rho \frac{\partial^2 u}{\partial t^2} = G \frac{\partial^2 u}{\partial z^2} + \eta \frac{\partial^3 u}{\partial z^2 \partial t}$$

$$u(0, t) = \underline{\exp(i\omega t)}; \quad \frac{\partial u}{\partial z}(L, t) = \underline{0}$$

$$u(z, t) = \underline{\phi(z)} \exp(i\omega t)$$

$$\Rightarrow -\rho\omega^2 \phi \exp(i\omega t) = G\phi'' \exp(i\omega t) + i\eta\omega\phi'' \exp(i\omega t)$$

$$\Rightarrow \phi''(G + i\eta\omega) + \rho\omega^2 \phi = 0$$

$$\Rightarrow \underline{\phi'' + \lambda^2 \phi = 0}; \quad \lambda^2 = \frac{\rho\omega^2}{(G + i\eta\omega)}$$

$$\phi(0) = \underline{1}$$
$$\phi'(L) = 0$$

$$\phi(z) = A \cos \lambda z + B \sin \lambda z$$

$$\underline{\phi(0) = 1} \quad \phi'(L) = 0$$

$$\Rightarrow \phi(x) = \cos \lambda z + \tan \lambda L \sin \lambda z \quad \checkmark$$

$$\underline{\phi(L)} = \frac{1}{\cos \lambda L} = \frac{1}{\cos\left(\frac{\omega L}{v^*}\right)}$$
$$v^* = \sqrt{\frac{G^*}{\rho}} = \sqrt{\frac{G(1+i\omega\eta)}{\rho}} = \sqrt{\frac{G(1+2i\xi)}{\rho}}$$

