<u>Lecture – 19</u>

## Stability of Linear Time Invariant Systems

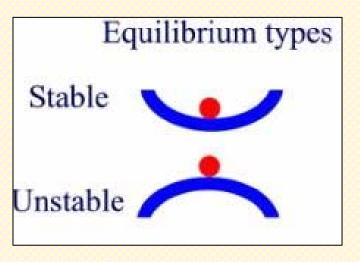
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# **Stability of Linear Systems**

**Definition**: If a system in equilibrium is disturbed and the system returns back to the equilibrium point with time, then the equilibrium point is said to be stable.



## **Stability of Linear Time Invariant (LTI) Systems**

System:

$$\dot{X} = AX, \quad X(0) = X_0$$

**Question:** 

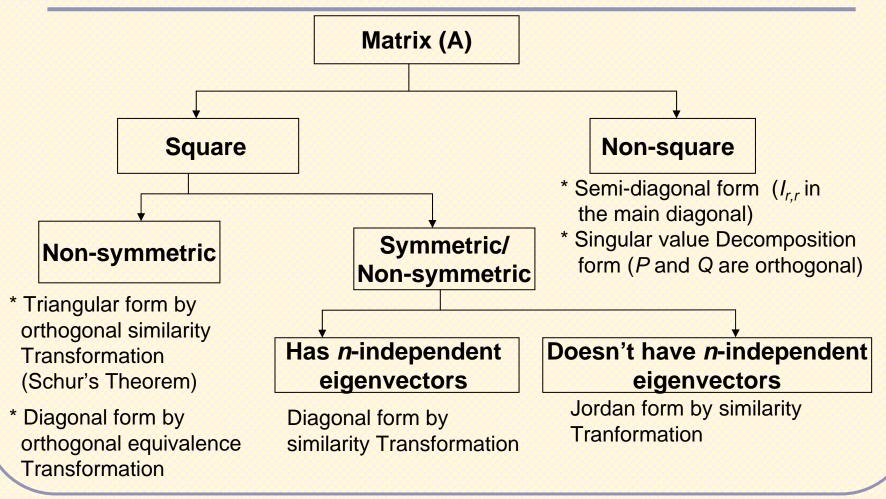
Can we conclude about nature of the solution, without solving the system model?

Answer: YES!

Definition: Eigenvalues of A : "Poles" of the system!

The nature of the solution is governed only by the locations of its poles

## **Summary of Matrix Transformations**



# **Similarity Transformation**

**Definition:** If  $A_{n \times n}$  and  $B_{n \times n}$  are nonsingular matrices and  $P_{n \times n}$  is a non-singular matrix such that  $B = P^{-1}AP$ , then *A* and *B* are "similar".

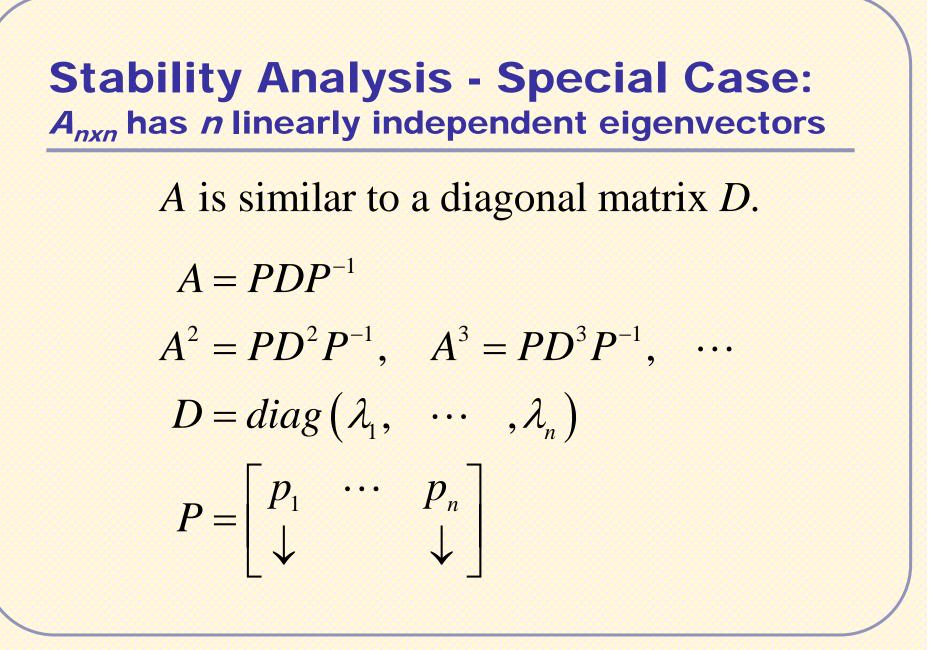
## Simplest forms possible:

Diagonal form

(if there are *n* linearly independent eigenvectors)

#### Jordan form

(if the number of linearly independent eigenvectors are less then *n*)



## **Special Case:** *A<sub>nxn</sub>* has *n* linearly independent eigenvectors

# Solution: $X(t) = e^{At} X_0$ $= \left( I + At + A^{2}t^{2} / 2! + A^{3}t^{3} / 3! + \cdots \right) X_{0}$ $= \left( PP^{-1} + PDP^{-1}t + PD^{2}P^{-1}t^{2} / 2! + \cdots \right) X_{0}$ $= P(I + Dt + D^{2}t^{2} / 2! + \cdots)P^{-1}X_{0}$ $= P(e^{Dt})P^{-1}X_0$ $= P \left[ diag \left( 1 + \lambda_i t + \lambda_i^2 t^2 / 2! + \cdots \right) \right] C$

## **Special Case:** *A<sub>nxn</sub>* has *n* linearly independent eigenvectors

Solution:

$$X(t) = \sum_{i=1}^{n} c_i e^{\lambda_i t} p_i \quad \text{(Modal form)}$$

**Conclusion** 

The nature of solution depends only on the location of poles!

All poles in the LH plane:Stable SystemOne pole in the RH plane:Unstable System

A is similar to a block-diagonal Jordan matrix J.  $J = diag(J_1, \dots, J_p)$  $A = P.IP^{-1}$  $A^{2} = PJ^{2}P^{-1}, \quad A^{3} = PJ^{3}P^{-1}, \quad \cdots$  $J^2 = diag(J_1^2, \cdots, J_p^2)$  $J^3 = diag(J_1^3, \dots, J_p^3)$ 

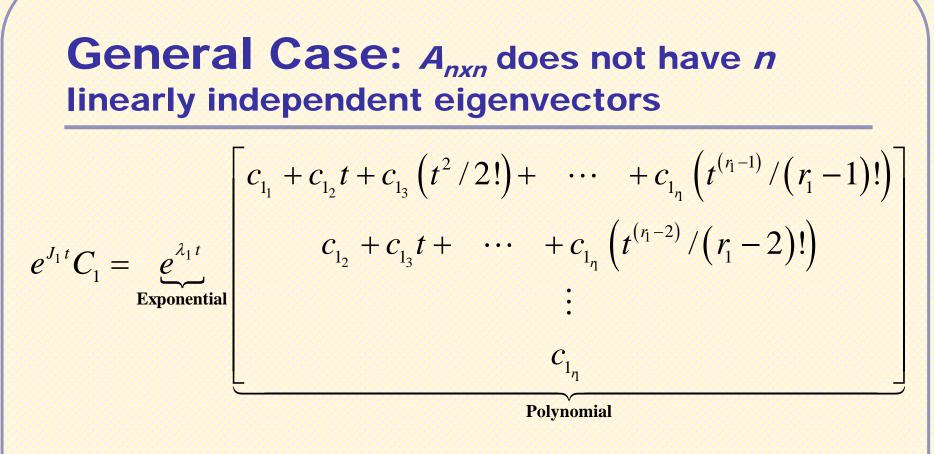
Solution:  $X(t) = e^{At} X_0$  $= \left( I + At + A^{2}t^{2} / 2! + A^{3}t^{3} / 3! + \cdots \right) X_{0}$  $= \left( PP^{-1} + PJP^{-1}t + PJ^2P^{-1}t^2 / 2! + \cdots \right) X_0$  $= P(I + Jt + J^{2}t^{2} / 2! + \cdots)P^{-1}X_{0}$  $= P(e^{Jt})P^{-1}X_0$  $e^{Jt} = diag\left(e^{J_1t}, \cdots, e^{J_pt}\right)$ 

Let  $\hat{J}$  be a particular  $r \times r$  Jordan block with eigenvalue  $\lambda$  $\hat{J}t = \lambda t I + Et$ 

$$E = \begin{bmatrix} 0 & 1 & 0 & \cdots & 0 \\ 0 & 0 & 1 & \ddots & \vdots \\ 0 & 0 & 0 & \ddots & 0 \\ \vdots & \ddots & \ddots & \ddots & 1 \\ 0 & 0 & 0 & \cdots & 0 \end{bmatrix}, \quad E^{2} = \begin{bmatrix} 0 & 0 & 1 & \cdots & 0 \\ 0 & 0 & 0 & \ddots & 1 \\ \vdots & \ddots & \ddots & \ddots & 0 \\ 0 & 0 & 0 & \cdots & 0 \end{bmatrix}, \quad \cdots \quad E^{r-1} = \begin{bmatrix} 0 & 0 & 0 & \cdots & 1 \\ 0 & 0 & 0 & \ddots & 0 \\ \vdots & \ddots & \ddots & \ddots & 0 \\ 0 & 0 & 0 & \cdots & 0 \end{bmatrix}$$
$$E^{r} = E^{r+1} = \cdots = 0$$

$$e^{\hat{j}t} = e^{\lambda t} \begin{bmatrix} 1 & t & \frac{1}{2!}t^2 & \cdots & \frac{1}{(r-1)!}t^{r-1} \\ 0 & 1 & t & \ddots & \vdots \\ 0 & 0 & \ddots & \ddots & \frac{1}{2!}t^2 \\ \vdots & \vdots & \ddots & 1 & t \\ 0 & \cdots & 0 & 0 & 1 \end{bmatrix}$$
$$X(t) = e^{At}X_0 = Pe^{Jt}C = \begin{bmatrix} p_1 & \cdots & p_p \\ \downarrow & & \downarrow \end{bmatrix} \begin{bmatrix} e^{J_1t}C_1 \\ \vdots \\ e^{J_pt}C_p \end{bmatrix}$$

> Let  $\lambda_1$  be repeated  $r_1$  times. Then  $C_1 = \begin{bmatrix} c_{1_1} & \cdots & c_{1_n} \end{bmatrix}^T$  $P_1 = \begin{vmatrix} p_1 & p_2 & \cdots & p_{r_1} \\ \downarrow & \downarrow & \downarrow & \downarrow \end{vmatrix}$  $p_1$ : Eigenvector  $p_2, \dots, p_n$ : Generalized Eigenvectors



Similar expressions can be obtained for  $P_i e^{J_i t} c_i$ ,  $i = 2, 3, \cdots$ 

Exponential term will eventually dominate the polynomial term!

## **Stability of Linear Systems**

#### **Conclusion**

The nature of solution depends only on the location of poles!

All poles in the LH plane:Stable SystemOne pole in the RH plane:Unstable System

# **Stabilizing Control Design**

Closed loop system:  $\dot{X} = AX + BU$ U = -KX $\dot{V} = AX + BU$ 

- $X = A_{CL}X$ , where  $A_{CL} = (A BK)$
- Closed loop system is stable if Eigenvalues of A<sub>CL</sub> satisfy the stability condition
- > For stabilizing controller K needs to be selected in such a way that the eigenvalues of  $A_{CL}$  should be in the left half plane



## Controllability of Linear Time Invariant Systems

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## Controllability

A system is said to be *controllable* at time t<sub>0</sub> if it is possible by means of an *unconstrained control vector* to transfer the system from any initial state x<sub>0</sub> to any other state *in a finite interval of time*

Controllability depends upon the system matrix

A and the control influence matrix B

# **Condition for Controllability:** (single input case)

System:  $\dot{X} = AX + Bu$ 

Solution:  $X(t) = e^{At}X(0) + \int_{0}^{t} e^{A(t-\tau)}Bu(\tau) d\tau$ 

Assuming 
$$X(t_1) = 0$$
,  
 $0 = e^{At_1} X(0) + \int_0^{t_1} e^{A(t_1 - \tau)} B u(\tau) d\tau$   
 $X(0) = -\int_0^{t_1} e^{-A\tau} B u(\tau) d\tau$ 

# **Condition for Controllability:** (single input case)

 $e^{-A\tau} = \sum_{k=1}^{n-1} \alpha_{k}(\tau) A^{k}$  (Sylvester's formula)  $X(0) = -\int_{0}^{t_{1}} e^{-A\tau} Bu(\tau) d\tau = -\sum_{k=0}^{n-1} A^{k} B \int_{0}^{t_{1}} \alpha_{k}(\tau) u(\tau) d\tau$  $= -\sum_{k=0}^{n-1} A^k B \beta_k \qquad \text{where} \quad \beta_k \triangleq \int_0^{t_1} \alpha_k(\tau) u(\tau) d\tau$  $= -\begin{bmatrix} B & AB & \cdots & A^{n-1}B \end{bmatrix} \begin{bmatrix} \beta_0 & \beta_1 & \cdots & \beta_{n-1} \end{bmatrix}^T$ This system should have a non-trivial solution for  $\begin{bmatrix} \beta_0 & \beta_1 & \cdots & \beta_{n-1} \end{bmatrix}^n$ 

## Controllability

**<u>Result</u>**: If the rank of  $C_B \triangleq \begin{bmatrix} B & AB & \cdots & A^{n-1}B \end{bmatrix}$  is *n*,

then the system is controllable.

Example:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 2 \\ 1 \end{bmatrix} u$$

$$C_B = \begin{bmatrix} 2 \\ 1 \end{bmatrix} \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix} \begin{bmatrix} 2 \\ 1 \end{bmatrix} = \begin{bmatrix} 2 & -2 \\ 1 & -2 \end{bmatrix}$$

 $rank(C_B) = 2$  ... The system is controllable.

## **Output Controllability**

Result:	$\dot{X} = AX + BU$

Y = CX + DU

 $X \in \mathbb{R}^n$ ,  $U \in \mathbb{R}^m$ ,  $Y \in \mathbb{R}^p$ If the rank of  $C_B \triangleq \begin{bmatrix} CB & CAB & \cdots & CA^{n-1}B & D \end{bmatrix}$  is p, then the system is output controllable. Note: The presence of DU term in the output equation

always helps to establish output controllability.

### Observability of Linear Time Invariant Systems

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## **Observability**

• A system is said to be *observable* at time  $t_0$  if, with the system in state  $X(t_0)$ , it is possible to determine this state from the observation of the output over a finite interval of time

Observability depends upon the system matrix A and the output matrix C

ObservabilityResult:If the rank of 
$$O_B \triangleq \begin{bmatrix} C^T & A^T C^T & \cdots & (A^T)^{n-1} C^T \end{bmatrix}$$
 is  $n$ ,  
then the system is observable.Example: $\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 2 \\ 1 \end{bmatrix} u \quad y = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$  $O_B = \begin{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix} \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix} = \begin{bmatrix} 1 & -1 \\ 0 & 0 \end{bmatrix}$  $rank(O_B) = 1 \neq 2$ 

## **Controllability and Observability in Transfer Function Domain**

- The system is both controllable and observable if there is no Pole-Zero cancellation.
- Note: The cancelled pole-zero pair suppresses part of the information about the system

# **Principle of Duality**

System **S**<sub>1</sub>:  $\dot{X} = AX + BU$   $C_B = \begin{bmatrix} B & AB & A^2B & \cdots & A^{n-1}B \end{bmatrix}$  $Y_1 = CX$   $O_B = \begin{bmatrix} C^T & A^TC^T & A^{T^2}C^T & \cdots & A^{T^{n-1}}C^T \end{bmatrix}$ 

System S<sub>2</sub>:  $\dot{Z} = A^T Z + C^T V$   $C_B = \begin{bmatrix} C^T & A^T C^T & A^{T^2} C^T & \cdots & A^{T^{n-1}} C^T \end{bmatrix}$  $Y_2 = B^T Z$   $O_B = \begin{bmatrix} B & AB & A^2 B & \cdots & A^{n-1}B \end{bmatrix}$ 

The principle of duality states that the system  $S_1$  is controllable if and only if system  $S_2$  is observable; and vice-versa!

Hence, the problem of observer design for a system is actually a problem of control design for its dual system.

# **Stabilizability and Detectability**

- Stabilizable system: Uncontrollable system in which uncontrollable part is stable
- Detectable system: Unobservable system in which the unobservable subsystem is stable

Where do uncontrollable or unobservable systems arise?

Redundant state variables

Physically uncontrollable system

Too much symmetry

## References

 K. Ogata: Modern Control Engineering, 3<sup>rd</sup> Ed., Prentice Hall, 1999.

 B. Friedland: Control System Design, McGraw Hill, 1986.

