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## **In this lecture...**

- Axial flow turbine
	- Performance characteristics
	- Axial turbine blades

**TURBOMACHINERY AERODYNAMICS** 

• Exit flow matching with nozzle

## **Axial turbine performance**

• We have seen that for an axial compressor,

 $P_{02}$ ,  $\eta_c = f(\dot{m}, P_{01}$ ,  $T_{01}$ ,  $\Omega$ ,  $\gamma$ , R,  $\nu$ , design, D) In terms of non - dimensionless parameters,

$$
\frac{P_{02}}{P_{01}}\text{ , } \eta_{C}\text{ }=\text{ }f\text{ }\! \left(\frac{\dot{m}\sqrt{\gamma RT_{01}}}{P_{01}D^{2}}\text{ , } \frac{\Omega D}{\sqrt{\gamma RT_{01}}}\text{ , } \frac{\Omega D^{2}}{v}\text{ , } \gamma \text{ , } \text{ } \! \
$$

are fixed. Therefore the above reduces to affect the performance significantly. Also, D and R For a given design, we can assume that  $\gamma$  and v do not

$$
\frac{P_{02}}{P_{01}}\, , \, \eta_C \, = f\!\!\left(\frac{\dot{m}\sqrt{T_{01}}}{P_{01}}\, , \frac{N}{\sqrt{T_{01}}}\right)
$$

## **Axial turbine performance**

characteristics for a turbine as well. In a similar manner, we can define performance

fluid at a sufficiently high Reynolds number, Therefore, for a given turbine operating with a given

$$
\frac{P_{02}}{P_{01}}\, , \, \eta_C \, = f\!\!\left(\frac{\dot{m}\sqrt{T_{01}}}{P_{01}}\, , \frac{N}{\sqrt{T_{01}}}\right)
$$

the turbine, respectively. Where, subscripts 01 and 02 denote the inlet and exit of

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#### **Axial turbine performance**



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#### **Axial turbine performance**



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## **Axial turbine performance**

- The efficiency plot shows that it is constant over a wide range of rotational speeds and pressure ratios.
- This is because the accelerating nature of the flow permits turbine blades to operate with a wide range of incidence.
- Maximum mass flow is limited by choking of the turbine.
- The mass flow characteristics tend to merge into a single curve independent of speed, for larger number of stages.

## **Axial turbine performance**

- When the turbine operates close to its design point (low incidence), the performance curves can be reduced to a single curve.
- As the number of stages are increased, there is a noticeable tendency for the characteristic to become ellipsoidal.
- With increase in the number of stages, the choking mass flow also reduces.
- Stodola (1945) formulated the "ellipse law", which has been used extensively by designers.

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#### **Axial turbine performance**



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## **Axial turbine performance**

- The performance of turbines is limited by two factors:
	- Compressibility
	- Stress
	- Inlet temperature
- Compressibility limits the mass flow that can pass through a turbine.
- Stress limits the rotational speed.
- It is also known that the performance also strongly depends upon temperature.
- Temperature in turn affects the stress.
- Hence, in a design exercise, there must be a compromise between the maximum temperature and the maximum rotor speed.

## **Axial turbine performance**

- For a given pressure ratio and adiabatic efficiency, the turbine work per unit mass is proportional to the inlet stagnation temperature.
- Therefore typically a 1% increase in the turbine inlet temperature can produce 2-3% increase in the engine output.
- Therefore there are elaborate methods used for cooling the turbine nozzle and rotor blades.
- Turbine blades with cooling can withstand temperatures higher than that permissible by the blade materials.

## **Axial turbine blades**

- Blade shapes used in turbines are quite different from that used in compressors.
- The design of these blades depend upon the passage Mach number, stress levels and various other parameters.
- The thickness distributions, suction surface curvature and trailing edge shape are varied for particular applications.
- Turbine blades could be designed specifically for subsonic, transonic or supersonic Mach numbers.

## **Axial turbine blades**

- Profiles can be generally classified as:
	- Profiles derived from various agencies like NACA, AGARD etc.
	- Profiles with circular arc and parabolic arc camber.
	- Profiles derived graphically or empirically from a specified pressure or Mach number distribution.
	- Each industry has developed their own proprietary profiles to meet their requirements.
	- Recent trend towards custom-designed or custom-tailored airfoils.

#### **Axial turbine blades**



NACA basic turbine profiles



Profile for subsonic inlet and supersonic outlet



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#### **Axial turbine blades**



Typical steam turbine tip section airfoils



Profile for supersonic inlet and supersonic outlet

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#### **Axial turbine blades**



Pressure distribution around a typical turbine blade

## **Axial turbine blades**

- Spacing between blades is a critical parameter in turbomachine performance.
- Closer spacing means lower loading per blade, but more number of blades, increased weight and frictional losses.
- Larger spacing means higher blade loading and lower weight, losses etc.
- Optimum number of blades usually empirical.

 $\frac{c}{C}$  (tan $\alpha_1$  – tan $\alpha_2$ ) S cos  $\mathsf{V}_2^2\mathsf{C}$ This canbe simplified as  $Z = \frac{2F}{\sqrt{2}}$  $F_w$ :blade force; C:chord  $V_2^2C$ Zwifel (1945) criterion :  $Z = \frac{2F_w}{M^2C}$  F<sub>w</sub> W W 2  $\sim$   $\mu$ ana<sub>1</sub>  $\mu$ ana<sub>2</sub> 2 2 2 2 2  $\frac{2F_w}{\Delta t^2 \Omega} = 2\cos^2\alpha_2 \frac{S}{\Omega}$  (tan $\alpha_1$  – tan $\alpha$ (1945) criterion :  $Z = \frac{2}{2}$ ρ ρ  $=\frac{2\mathsf{i} \mathsf{w}}{1\mathsf{i} \mathsf{a}^2}$  = 2 cos<sup>2</sup>  $\alpha$ <sub>2</sub>  $\frac{3}{6}$  (tan $\alpha$ <sub>1</sub>  $-$ =

## **Axial turbine blades**

- There are several differences between the flow through a turbine blade passage as compared with a compressor:
	- Pressure drop in a turbine is much larger than the pressure rise in a compressor.
	- The flow turning in a compressor: 20°-35° whereas in a turbine: as high as 160<sup>o</sup>.
	- Turbine designer usually delays formation of shocks (to minimize losses); in a compressor shocks are one of the modes of deceleration.
	- Therefore transonic compressors usually have lower efficiency than transonic turbines.

- The operation of a turbine is affected by components upstream (compressor) and downstream (nozzle).
- The compressor and turbine performance characteristics form an important part of this performance matching.
- It was discussed earlier that turbines do not exhibit any significant variation in nondimensional mass flow with speed.
- However the turbine operating region is severely affected by the nozzle.

- The nozzle exit area has a significant influence on the off-design operation of a turbine and the engine in general.
- The operation of the nozzle under choked or unchoked condition also influences the matching.
- The similarity between the flow characteristic of a nozzle and a turbine is the fact that thermodynamically, both are flow expanders.
- The matching between the turbine and the nozzle is identical to that between a freeturbine / power-turbine and the main turbine.

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- Once the nozzle is choked, the nozzle nondimensional flow will reach its maximum value and will become independent of the nozzle pressure ratio and therefore the flight speed.
- This results in the turbine operating point getting fixed because of matching requirement between turbine and nozzle.
- Therefore, when the nozzle is choking, the equilibrium running line will be uniquely determined by the fixed turbine operating point and will independent of flight speed.

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#### **Exit flow matching**



Matching characteristics of turbine and nozzle

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- Most of the modern engines operate with choked nozzle during majority of the operation.
- Only when the engine is operating with a low thrust say, when preparing to land or taxiing, the nozzle may be un-choked.
- Therefore at low speeds too one must ensure that the matching is maintained as at low speeds, the operating line is closer to the surge line.

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**TURBOMACHINERY AERODYNAMICS** 

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#### **In the next lecture...**

• Tutorial on axial flow turbines