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In this lecture...

- Axial flow turbine
 - Performance characteristics
 - Axial turbine blades

TURBOMACHINERY AERODYNAMICS

• Exit flow matching with nozzle

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Axial turbine performance

• We have seen that for an axial compressor,

$$\begin{split} P_{02}\,,\,\eta_{C}\,=\,f(\dot{m},P_{01}\,,\,T_{01}\,,\,\Omega,\,\gamma,R\,,\,\nu,\,design,D)\\ \text{In terms of non - dimensionless parameters,} \end{split}$$

$$\frac{P_{02}}{P_{01}}, \eta_{C} = f\left(\frac{\dot{m}\sqrt{\gamma RT_{01}}}{P_{01}D^{2}}, \frac{\Omega D}{\sqrt{\gamma RT_{01}}}, \frac{\Omega D^{2}}{\nu}, \gamma, \text{design}\right)$$

For a given design, we can assume that γ and ν do not affect the performance significantly. Also, D and R are fixed. Therefore the above reduces to

$$\frac{\mathsf{P}_{02}}{\mathsf{P}_{01}}, \, \eta_{\mathsf{C}} \, = \, \mathsf{f}\!\left(\frac{\dot{\mathsf{m}}\sqrt{\mathsf{T}_{01}}}{\mathsf{P}_{01}}, \frac{\mathsf{N}}{\sqrt{\mathsf{T}_{01}}}\right)$$

Axial turbine performance

In a similar manner, we can define performance characteristics for a turbine as well.

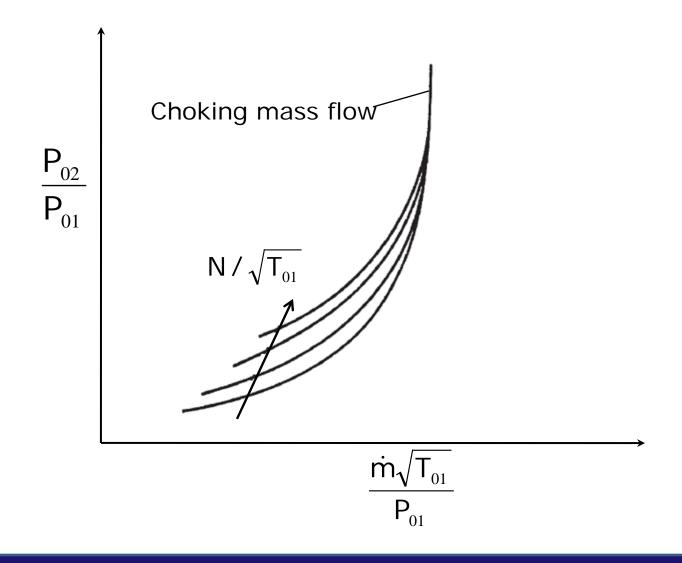
Therefore, for a given turbine operating with a given fluid at a sufficiently high Reynolds number,

$$\frac{P_{02}}{P_{01}}, \eta_{C} = f\left(\frac{\dot{m}\sqrt{T_{01}}}{P_{01}}, \frac{N}{\sqrt{T_{01}}}\right)$$

Where, subscripts 01 and 02 denote the inlet and exit of the turbine, respectively.

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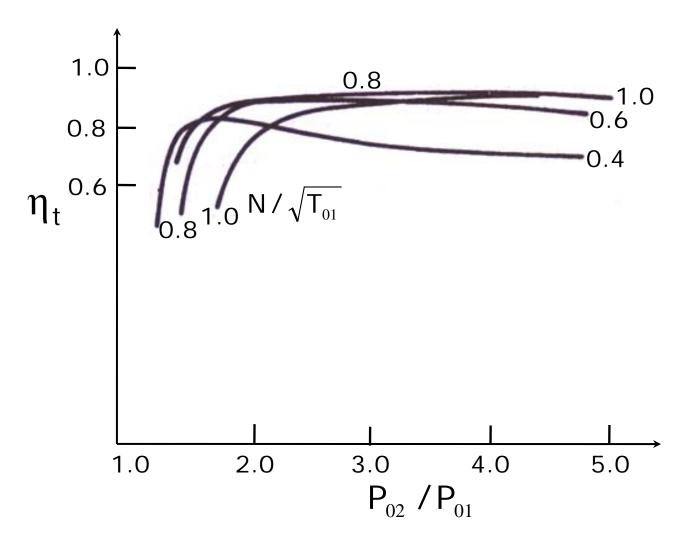
Axial turbine performance



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Axial turbine performance



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Axial turbine performance

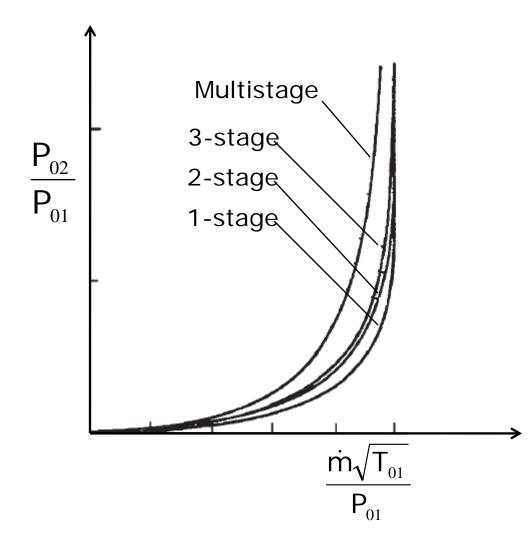
- The efficiency plot shows that it is constant over a wide range of rotational speeds and pressure ratios.
- This is because the accelerating nature of the flow permits turbine blades to operate with a wide range of incidence.
- Maximum mass flow is limited by choking of the turbine.
- The mass flow characteristics tend to merge into a single curve independent of speed, for larger number of stages.

Axial turbine performance

- When the turbine operates close to its design point (low incidence), the performance curves can be reduced to a single curve.
- As the number of stages are increased, there is a noticeable tendency for the characteristic to become ellipsoidal.
- With increase in the number of stages, the choking mass flow also reduces.
- Stodola (1945) formulated the "ellipse law", which has been used extensively by designers.

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Axial turbine performance



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Axial turbine performance

- The performance of turbines is limited by two factors:
 - Compressibility
 - Stress
 - Inlet temperature
- Compressibility limits the mass flow that can pass through a turbine.
- Stress limits the rotational speed.
- It is also known that the performance also strongly depends upon temperature.
- Temperature in turn affects the stress.
- Hence, in a design exercise, there must be a compromise between the maximum temperature and the maximum rotor speed.

Axial turbine performance

- For a given pressure ratio and adiabatic efficiency, the turbine work per unit mass is proportional to the inlet stagnation temperature.
- Therefore typically a 1% increase in the turbine inlet temperature can produce 2-3% increase in the engine output.
- Therefore there are elaborate methods used for cooling the turbine nozzle and rotor blades.
- Turbine blades with cooling can withstand temperatures higher than that permissible by the blade materials.

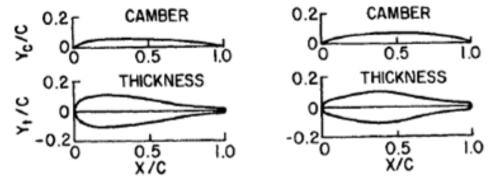
Axial turbine blades

- Blade shapes used in turbines are quite different from that used in compressors.
- The design of these blades depend upon the passage Mach number, stress levels and various other parameters.
- The thickness distributions, suction surface curvature and trailing edge shape are varied for particular applications.
- Turbine blades could be designed specifically for subsonic, transonic or supersonic Mach numbers.

Axial turbine blades

- Profiles can be generally classified as:
 - Profiles derived from various agencies like NACA, AGARD etc.
 - Profiles with circular arc and parabolic arc camber.
 - Profiles derived graphically or empirically from a specified pressure or Mach number distribution.
 - Each industry has developed their own proprietary profiles to meet their requirements.
 - Recent trend towards custom-designed or custom-tailored airfoils.

Axial turbine blades



NACA basic turbine profiles

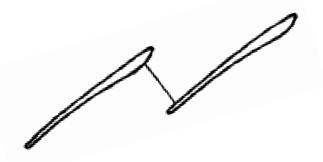


Profile for subsonic inlet and supersonic outlet

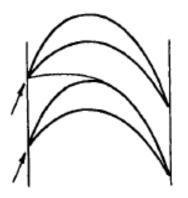


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Axial turbine blades



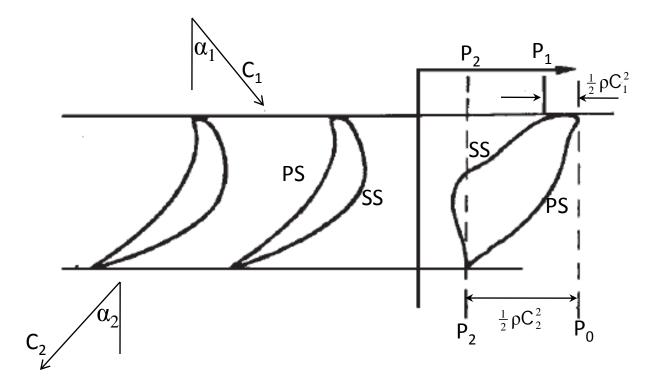
Typical steam turbine tip section airfoils



Profile for supersonic inlet and supersonic outlet

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Axial turbine blades



Pressure distribution around a typical turbine blade

Axial turbine blades

- Spacing between blades is a critical parameter in turbomachine performance.
- Closer spacing means lower loading per blade, but more number of blades, increased weight and frictional losses.
- Larger spacing means higher blade loading and lower weight, losses etc.
- Optimum number of blades usually empirical.

Zwifel (1945) criterion : $Z = \frac{2F_W}{\rho V_2^2 C}$ F_W : blade force; C : chord This canbe simplified as $Z = \frac{2F_W}{\rho V_2^2 C} = 2\cos^2 \alpha_2 \frac{S}{C}$ (tan $\alpha_1 - \tan \alpha_2$)

Axial turbine blades

- There are several differences between the flow through a turbine blade passage as compared with a compressor:
 - Pressure drop in a turbine is much larger than the pressure rise in a compressor.
 - The flow turning in a compressor: 20°-35° whereas in a turbine: as high as 160°.
 - Turbine designer usually delays formation of shocks (to minimize losses); in a compressor shocks are one of the modes of deceleration.
 - Therefore transonic compressors usually have lower efficiency than transonic turbines.

- The operation of a turbine is affected by components upstream (compressor) and downstream (nozzle).
- The compressor and turbine performance characteristics form an important part of this performance matching.
- It was discussed earlier that turbines do not exhibit any significant variation in nondimensional mass flow with speed.
- However the turbine operating region is severely affected by the nozzle.

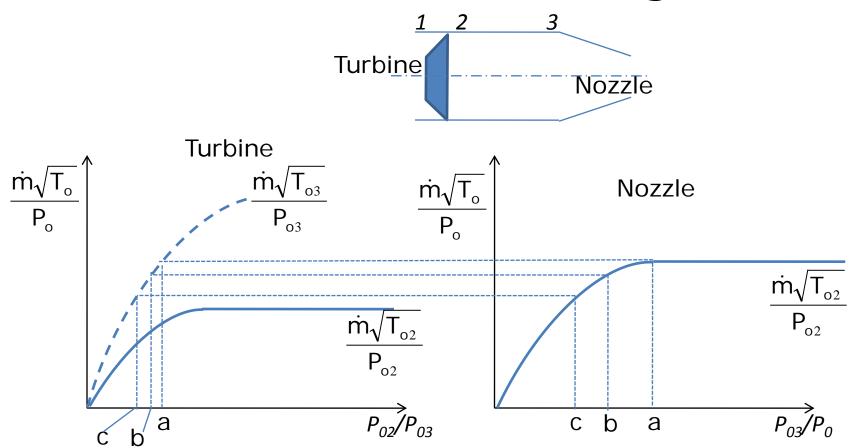
- The nozzle exit area has a significant influence on the off-design operation of a turbine and the engine in general.
- The operation of the nozzle under choked or unchoked condition also influences the matching.
- The similarity between the flow characteristic of a nozzle and a turbine is the fact that thermodynamically, both are flow expanders.
- The matching between the turbine and the nozzle is identical to that between a freeturbine / power-turbine and the main turbine.

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- Once the nozzle is choked, the nozzle nondimensional flow will reach its maximum value and will become independent of the nozzle pressure ratio and therefore the flight speed.
- This results in the turbine operating point getting fixed because of matching requirement between turbine and nozzle.
- Therefore, when the nozzle is choking, the equilibrium running line will be uniquely determined by the fixed turbine operating point and will independent of flight speed.

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Exit flow matching



Matching characteristics of turbine and nozzle

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- Most of the modern engines operate with choked nozzle during majority of the operation.
- Only when the engine is operating with a low thrust say, when preparing to land or taxiing, the nozzle may be un-choked.
- Therefore at low speeds too one must ensure that the matching is maintained as at low speeds, the operating line is closer to the surge line.

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In the next lecture...

• Tutorial on axial flow turbines