Lect- 11

# In this lecture...

- Performance characteristics of axial flow compressors
  - Single stage characteristics

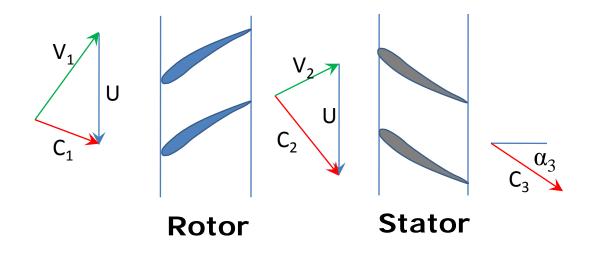
TURBOMACHINERY AERODYNAMICS

• Multi-stage characteristics

Lect-11

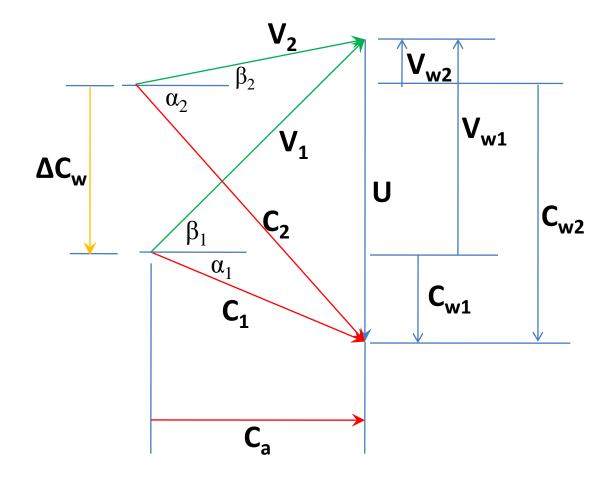
#### Single stage performance characteristics

 Let us consider a typical axial compressor stage comprising of a set of rotor blades followed by a set of stator blades.



Lect-11

#### Single stage performance characteristics



# Single stage performance characteristics

Lect-11

• From the above velocity triangles,

$$C_{w2} = U - C_a \tan \beta_2 \quad and \quad C_{w1} = C_a \tan \alpha$$
  
Since,  $\Delta h_0 = U \Delta C_w$   
 $\Delta h_0 = U [U - C_a (\tan \alpha_1 + \tan \beta_2)]$   
 $or, \quad \frac{\Delta C_w}{U} = \frac{\Delta h_0}{U^2} = 1 - \frac{C_a}{U} (\tan \alpha_1 + \tan \beta_2)$ 

# Single stage performance characteristics

- Change in the design mass flow rate affects  $C_{a'}$  change in rotor speed affects U.
- Change of either  $C_a$  or U changes the inlet angle  $\beta_1$  at which the flow approaches the rotor.
- The above equation shows that the blade performance depends upon the ratio  $C_a/U$ .

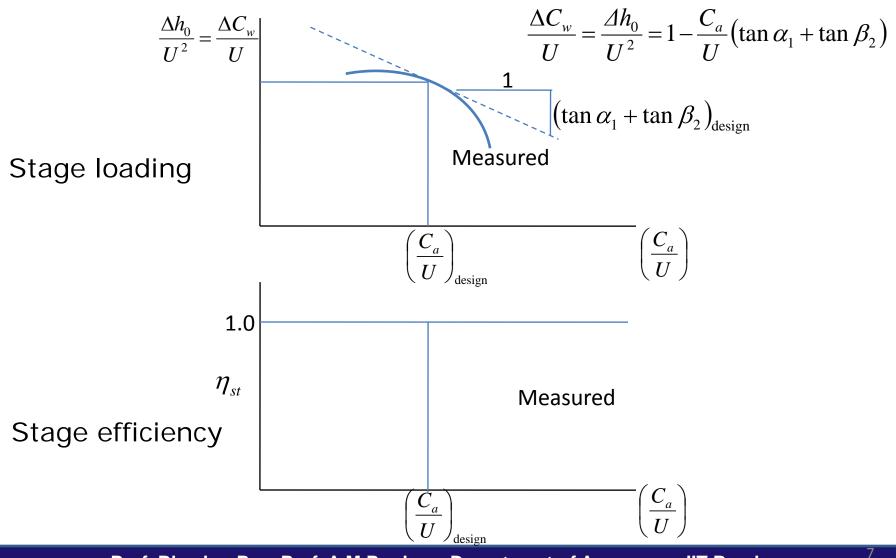
The stage performance is a function of the loading coefficient, flow coefficient and the efficiency.

Thus,

```
Stage performance = f(\psi, \phi, \eta)
```

Lect-11

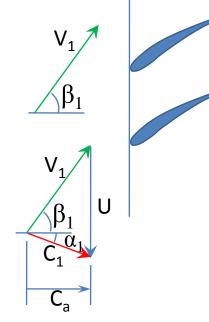
#### Single stage performance characteristics



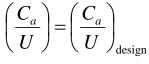
 $V_1$ 

Lect-11

# Single stage performance characteristics



Design condition : Normal operation



Off - design condition : Positive incidence flow separation

$$\left(\frac{C_a}{U}\right) < \left(\frac{C_a}{U}\right)_{\text{design}}$$

$$V_{1}$$

$$\beta_{1}$$

$$V_{1}$$

$$V_{1}$$

$$C_{1}$$

$$U$$

$$C_{1}$$

Off - design condition :

Negative incidence flow separation

$$\left(\frac{C_a}{U}\right) > \left(\frac{C_a}{U}\right)_{\text{design}}$$

- Let us know consider a multi-stage compressor. Inlet station is denoted by 1 and exit of the compressor by 2.
- Therefore the overall pressure ratio of the compressor is  $P_{02}/P_{01}$ .
- The compressor outlet pressure,  $P_{02}$ , and the isentropic efficiency,  $\eta_{C_{i}}$  depend upon several physical variables

# Multi-stage performance characteristics

Lect-11

$$P_{02}, \eta_C = f(\dot{m}, P_{01}, T_{01}, \Omega, \gamma, R, \nu, \text{design}, D)$$

In terms of non - dimensionless parameters,

$$\frac{P_{02}}{P_{01}}, \eta_C = f\left(\frac{\dot{m}\sqrt{\gamma RT_{01}}}{P_{01}D^2}, \frac{\Omega D}{\sqrt{\gamma RT_{01}}}, \frac{\Omega D^2}{\nu}, \gamma, \text{design}\right)$$

For a given design, we can assume that  $\gamma$  and  $\nu$  do not affect the performance significantly. Also, *D* and *R* are fixed. Therefore the above reduces to

$$\frac{P_{02}}{P_{01}}, \eta_C = f\left(\frac{\dot{m}\sqrt{T_{01}}}{P_{01}}, \frac{N}{\sqrt{T_{01}}}\right)$$

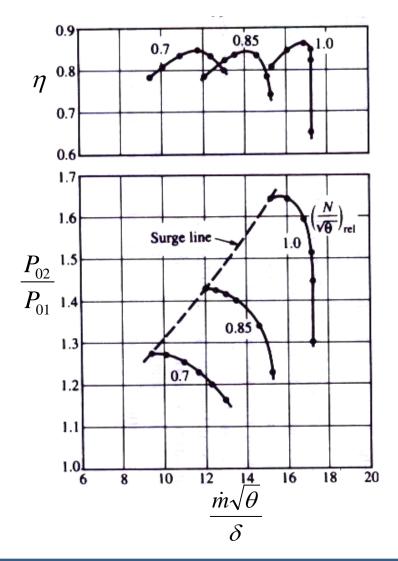
#### Multi-stage performance characteristics

Usually, this is further processed in terms of the standard day pressure and temperature.

$$\frac{P_{02}}{P_{01}}, \eta_{C} = f\left(\frac{\dot{m}\sqrt{\theta}}{\delta}, \frac{N}{\sqrt{\theta}}\right)$$
Where,  $\theta = \frac{T_{01}}{(T_{01})_{\text{Std. day}}}$  and  $\delta = \frac{P_{01}}{(P_{01})_{\text{Std. day}}}$ 
 $(T_{01})_{\text{Std. day}} = 288.15 \, K \text{ and } (P_{01})_{\text{Std. day}} = 101.325 \, kPa$ 

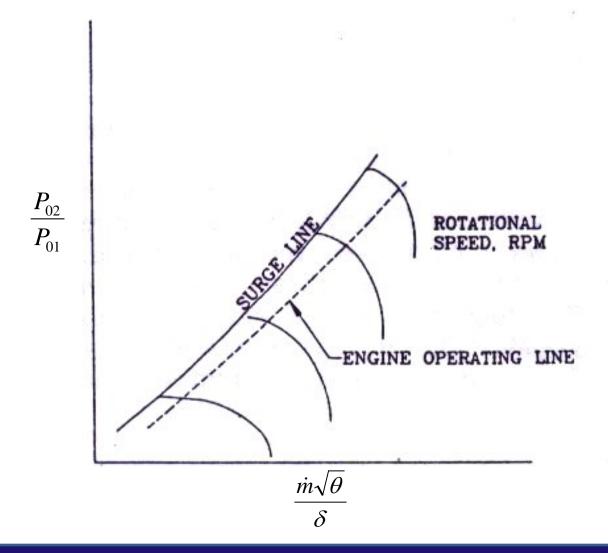
#### Multi-stage performance characteristics

Lect-11



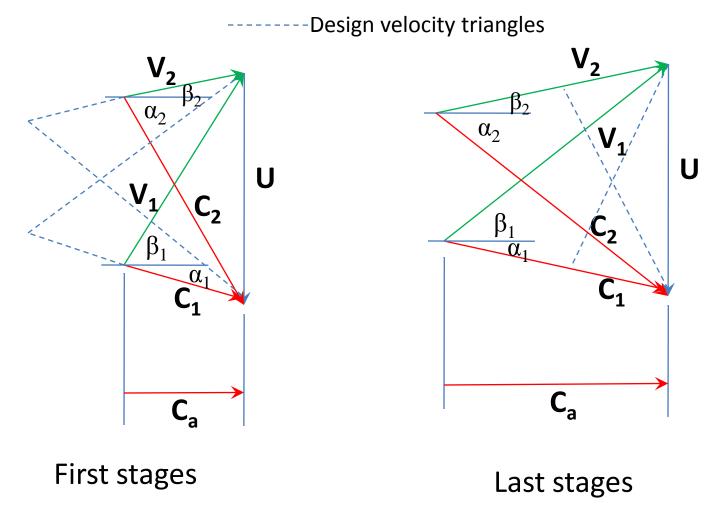
Lect-11

#### Multi-stage performance characteristics



- In a multi-stage compressor, a small departure from the design point at the first stage causes progressively increasing departure from design conditions from the first stage onwards.
- Thus, a small reduction in (c<sub>a</sub>/U)<sub>design</sub> at the first stage could lead to positive incidence separation at the last stage.
- Similarly, a small increase in (c<sub>a</sub>/U)<sub>design</sub> could lead to negative incidence separation in the last stage.
- The most extreme mismatching of the front and rear stages occur during starting.

Lect-11



- Decreased C<sub>a</sub> with α<sub>1</sub> and β<sub>2</sub> constant, results in increased α<sub>2</sub> and β<sub>1</sub> or increased loading on both rotor and stator blades.
- In the case of increased C<sub>a</sub>, it results in the opposite effect.
- Designers use several solutions to allow compressors to self-start: use of bleed valves allowing some of the incoming air to escape, variable IGVs, multi-spooling.

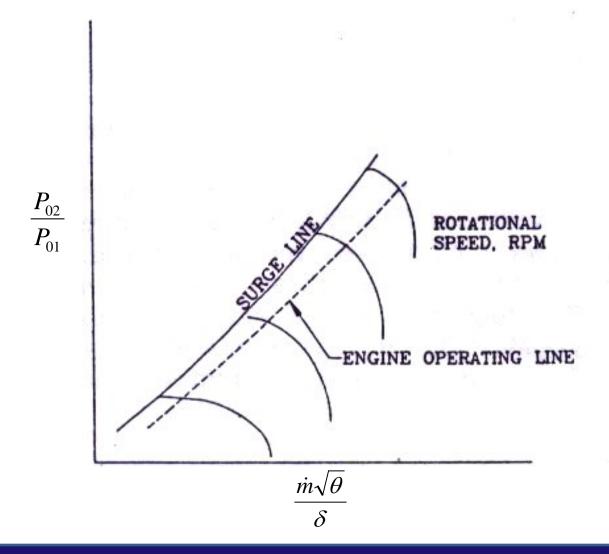
# Multi-stage performance characteristics

Lect-11

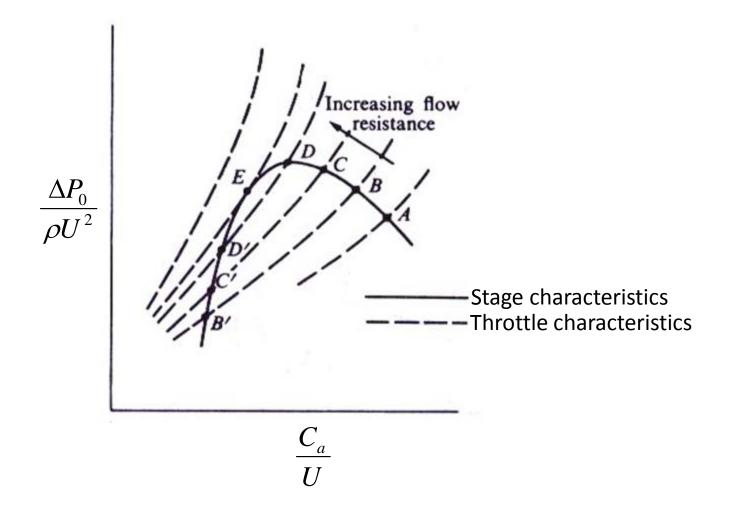
- Axial compressors suffer from two possible modes of unstable operation
  - Rotating stall: non-axisymmetric, aperiodic
  - Surge: axisymmetric, periodic
- Rotating stall: progression around the blade annulus of a stall pattern, in which one or more adjacent blade passages are instantaneously stalled, then are cleared for unstalled flow as the stall cell progresses.
- Rotating stall causes alternate loading and unloading of the blades: fatigue failure.

Lect-11

#### Multi-stage performance characteristics



Lect-11



# In this lecture...

- Performance characteristics of axial flow compressors
  - Single stage characteristics

TURBOMACHINERY AERODYNAMICS

• Multi-stage characteristics