



Jet Aircraft Propulsion

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Lect-16

In this lecture...

- Free vortex theory
- Single and multi-stage axial compressor characteristics

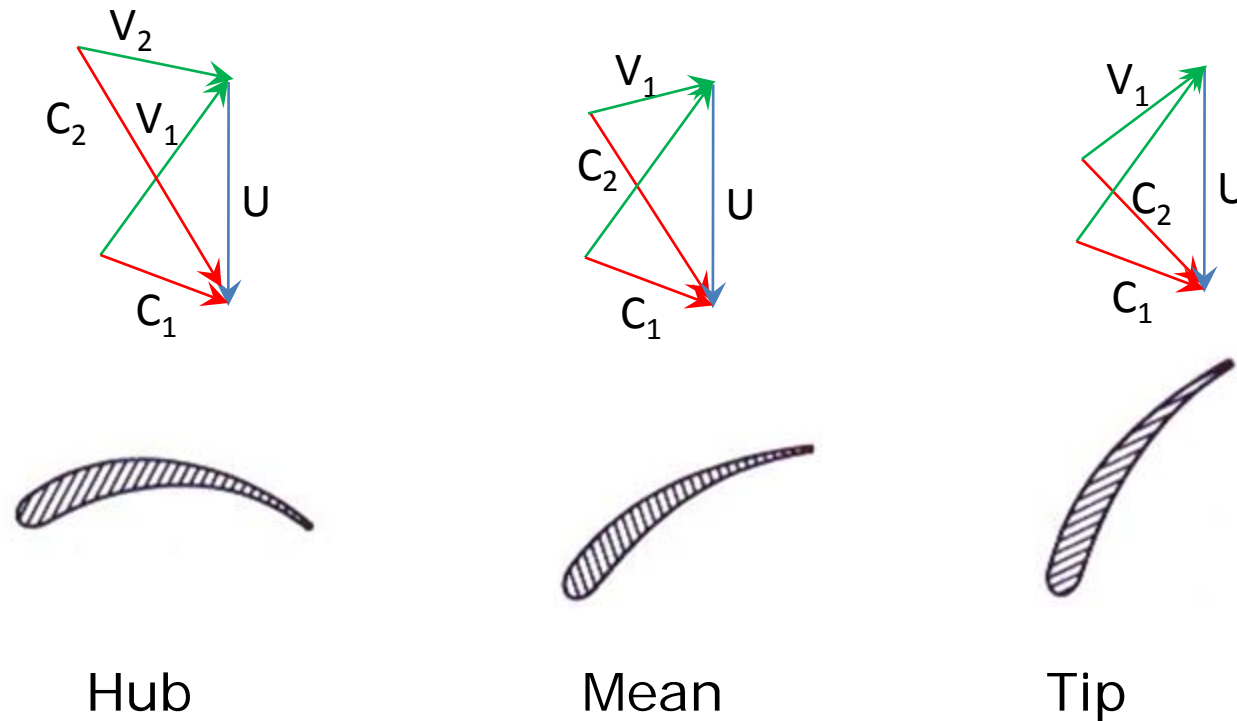
Radial equilibrium

- For a realistic design of an axial compressor blade, it is necessary to take into account radial variations in
 - Blade speed, U
 - Axial velocity, C_a
 - Tangential velocity, C_w
 - Static pressure
- Maintain a reasonably uniform flow at the exit of the compressor → uniform radial work input

Free vortex design

- Since $\Delta h_o = U\Delta C_\theta = \Omega r\Delta C_\theta$
- This means that for a given rotational speed, $r\Delta C_\theta$ must be a constant.
- One such configuration that satisfies the above is the Free Vortex Design.
- In this approach, the product rC_θ is held a constant across the exit of each blade row.
- From the axial velocity and the blade speeds at various radial sections, the velocity triangle can be completed.

Free vortex design



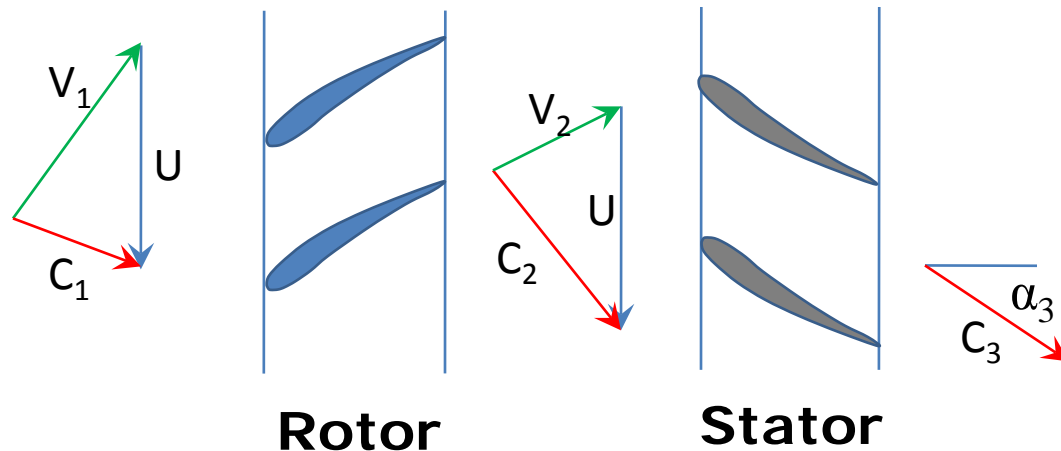
Free vortex velocity diagrams at the hub, mean and tip sections

Free vortex design

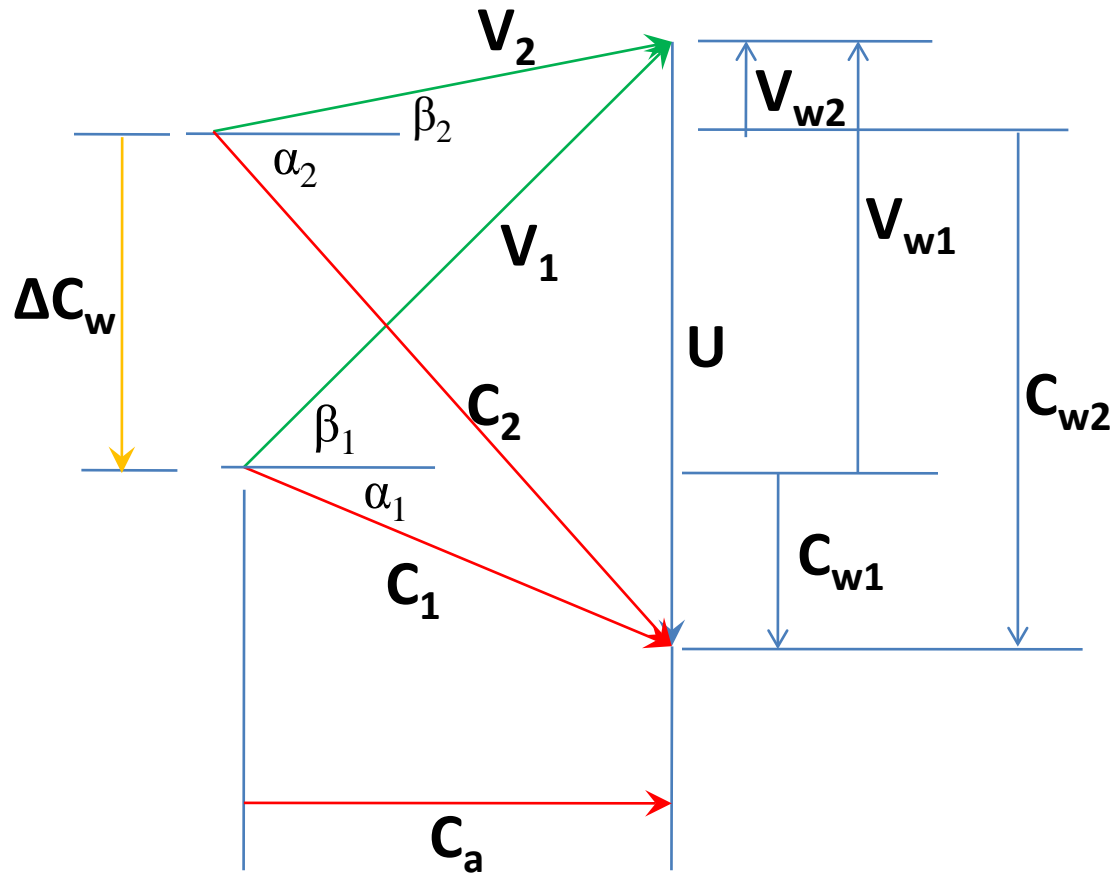
- The conditions of radial equilibrium, i.e., the satisfaction of the three-dimensional equations of fluid motion must be considered.
- Possible distributions that satisfy the constant specific radial work criterion are:
 - Free vortex, $rC_\theta = a$
 - Forced vortex, $rC_\theta = ar^2$
 - Exponential, $rC_\theta = ar + b$
 - Constant reaction, $rC_\theta = ar^2 + b$

Single stage performance characteristics

- Let us consider a typical axial compressor stage comprising of a set of rotor blades followed by a set of stator blades.



Single stage performance characteristics



Single stage performance characteristics

- From the above velocity triangles,

$$C_{w2} = U - C_a \tan \beta_2 \quad \text{and} \quad C_{w1} = C_a \tan \alpha$$

Since, $\Delta h_0 = U \Delta C_w$

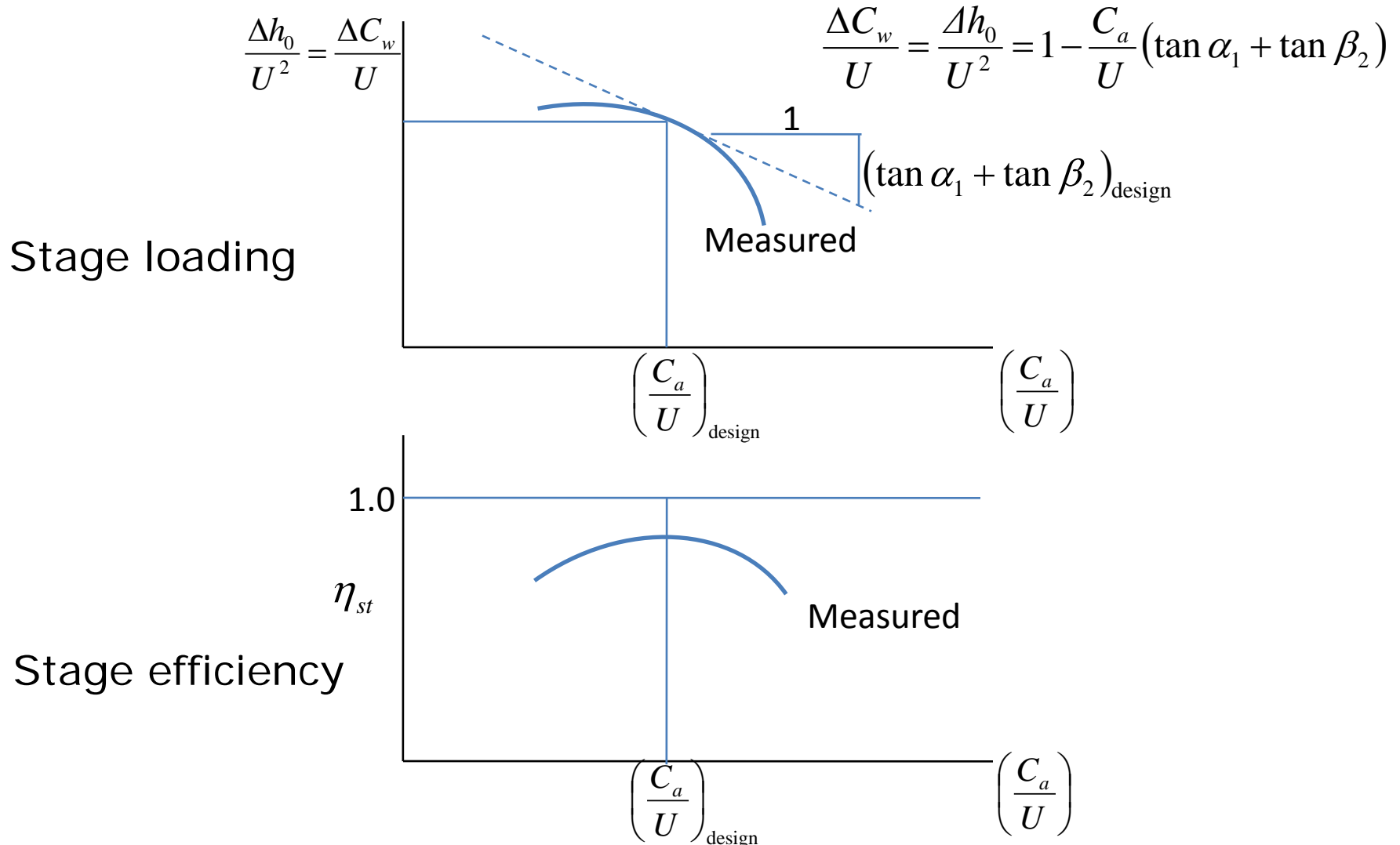
$$\Delta h_0 = U [U - C_a (\tan \alpha_1 + \tan \beta_2)]$$

$$\text{or, } \frac{\Delta C_w}{U} = \frac{\Delta h_0}{U^2} = 1 - \frac{C_a}{U} (\tan \alpha_1 + \tan \beta_2)$$

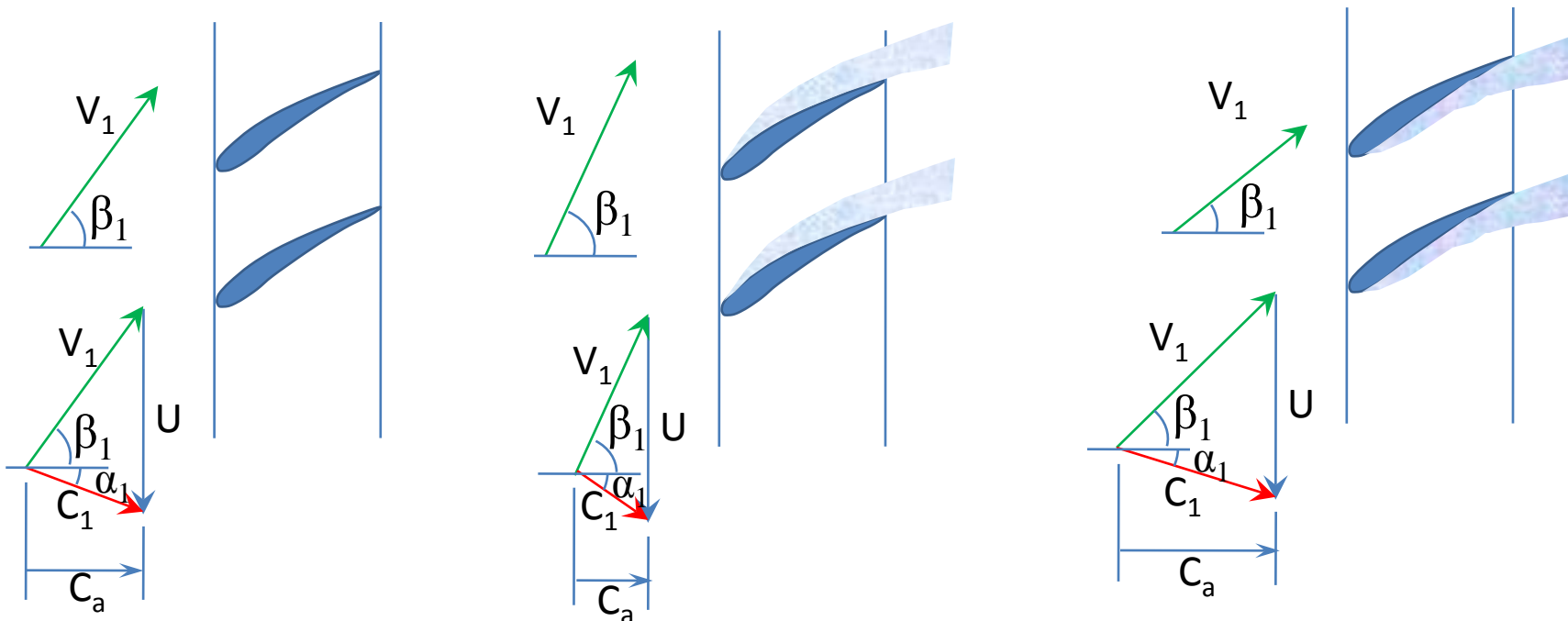
Single stage performance characteristics

- Change in the design mass flow rate affects C_a , change in rotor speed affects U .
- Change of either C_a or U changes the inlet angle β_1 at which the flow approaches the rotor.
- The above equation shows that the blade performance depends upon the ratio C_a/U .

Single stage performance characteristics



Single stage performance characteristics



Design condition :
Normal operation

$$\left(\frac{C_a}{U}\right) = \left(\frac{C_a}{U}\right)_{design}$$

Off - design condition :
Positive incidence flow separation

$$\left(\frac{C_a}{U}\right) < \left(\frac{C_a}{U}\right)_{design}$$

Off - design condition :
Negative incidence flow separation

$$\left(\frac{C_a}{U}\right) > \left(\frac{C_a}{U}\right)_{design}$$

Multi-stage performance characteristics

- Let us now consider a multi-stage compressor. Inlet station is denoted by 1 and exit of the compressor by 2.
- Therefore the overall pressure ratio of the compressor is P_{02}/P_{01} .
- The compressor outlet pressure, P_{02} , and the isentropic efficiency, η_C , depend upon several physical variables

$$P_{02}, \eta_C = f(\dot{m}, P_{01}, T_{01}, \Omega, \gamma, R, \nu, \text{design}, D)$$

Multi-stage performance characteristics

$$P_{02}, \eta_C = f(\dot{m}, P_{01}, T_{01}, \Omega, \gamma, R, \nu, \text{design}, D)$$

In terms of non - dimensionless parameters,

$$\frac{P_{02}}{P_{01}}, \eta_C = f\left(\frac{\dot{m}\sqrt{\gamma RT_{01}}}{P_{01}D^2}, \frac{\Omega D}{\sqrt{\gamma RT_{01}}}, \frac{\Omega D^2}{\nu}, \gamma, \text{design}\right)$$

For a given design, we can assume that γ and ν do not affect the performance significantly. Also, D and R are fixed. Therefore the above reduces to

$$\frac{P_{02}}{P_{01}}, \eta_C = f\left(\frac{\dot{m}\sqrt{T_{01}}}{P_{01}}, \frac{N}{\sqrt{T_{01}}}\right)$$

Multi-stage performance characteristics

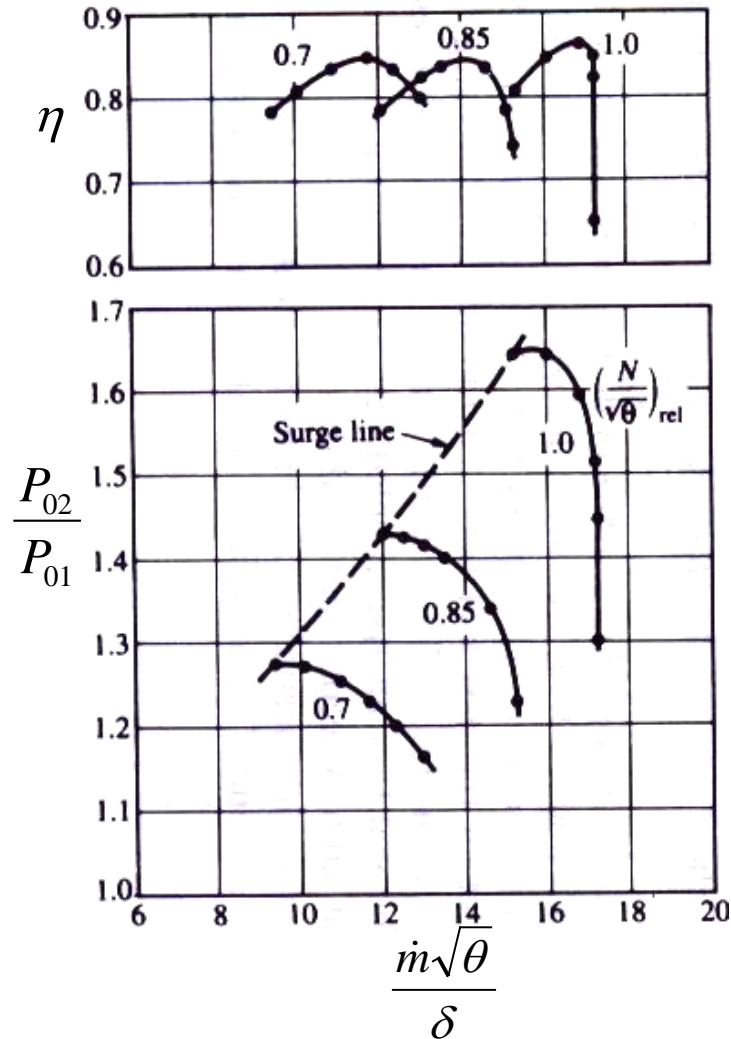
Usually, this is further processed in terms of the standard day pressure and temperature.

$$\frac{P_{02}}{P_{01}}, \eta_c = f\left(\frac{\dot{m}\sqrt{\theta}}{\delta}, \frac{N}{\sqrt{\theta}}\right)$$

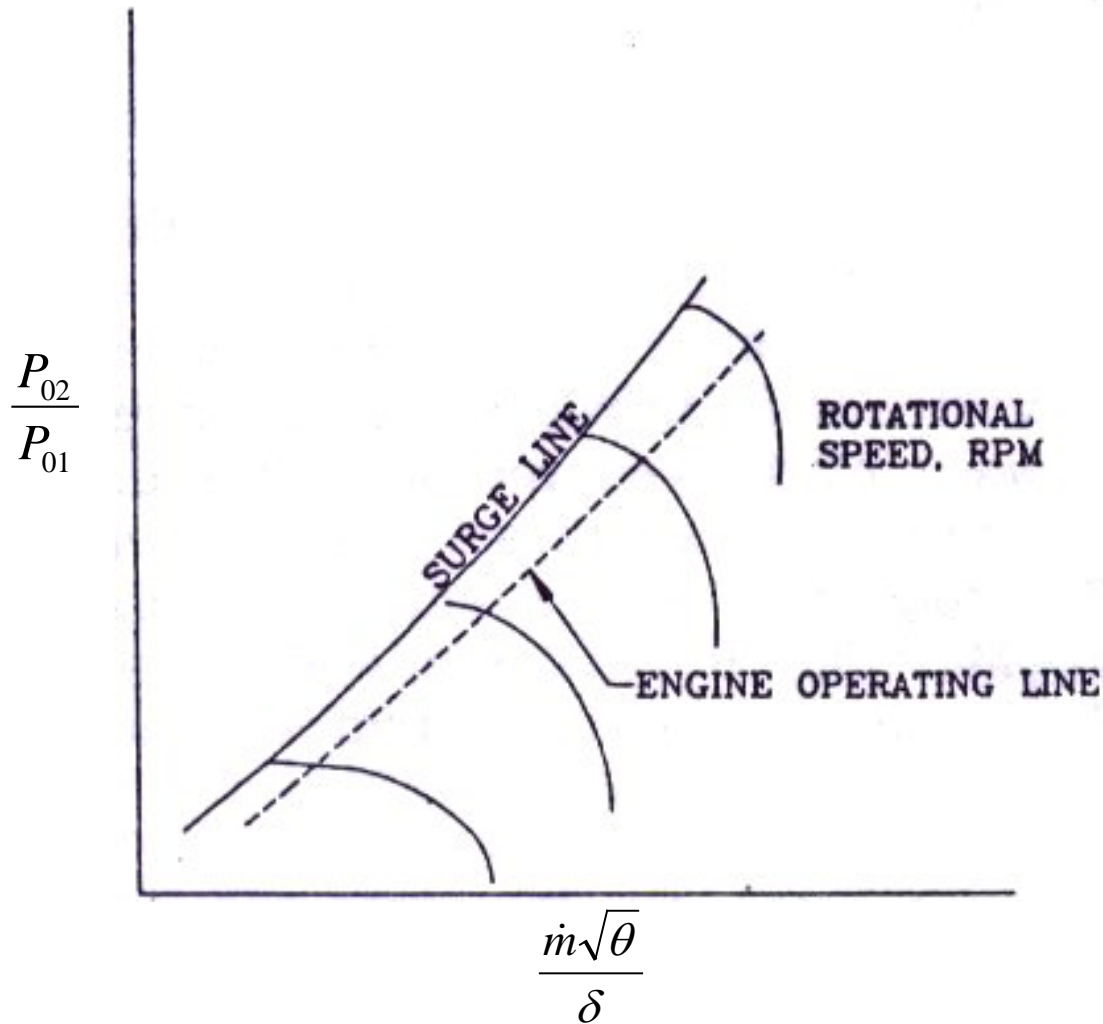
$$\text{Where, } \theta = \frac{T_{01}}{(T_{01})_{\text{Std. day}}} \quad \text{and} \quad \delta = \frac{P_{01}}{(P_{01})_{\text{Std. day}}}$$

$$(T_{01})_{\text{Std. day}} = 288.15 \text{ K} \quad \text{and} \quad (P_{01})_{\text{Std. day}} = 101.325 \text{ kPa}$$

Multi-stage performance characteristics



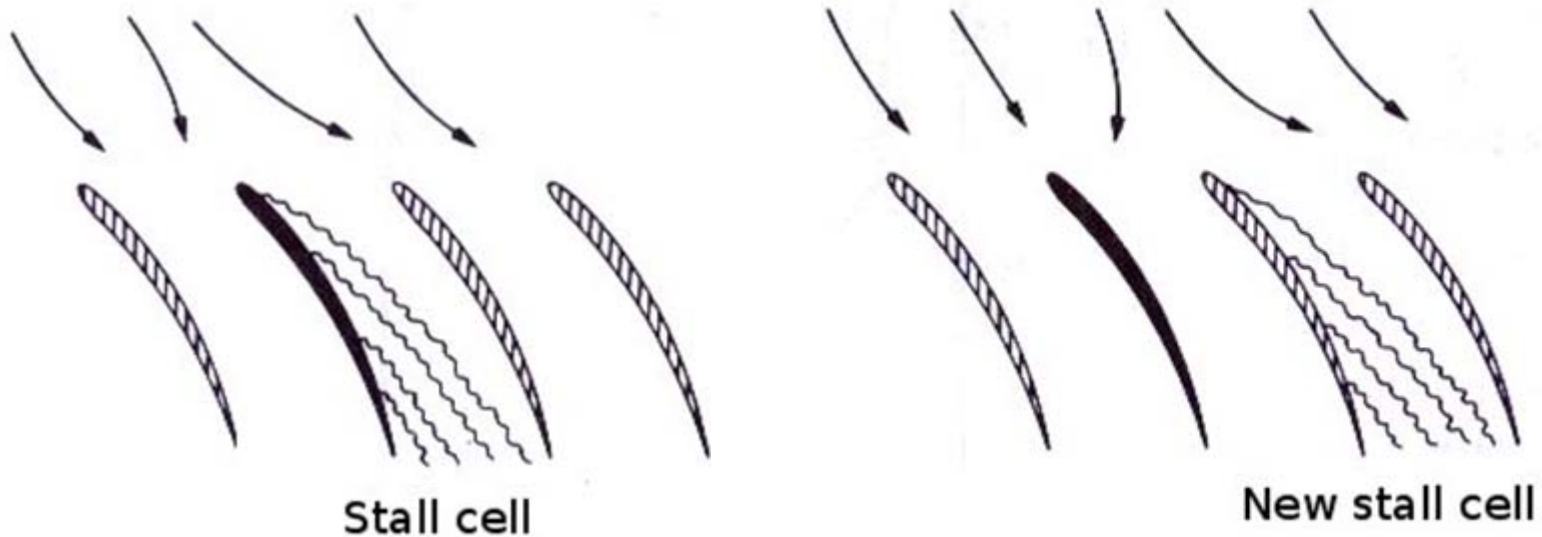
Multi-stage performance characteristics



Multi-stage performance characteristics

- Axial compressors suffer from two possible modes of unstable operation
 - Rotating stall: non-axisymmetric, aperiodic
 - Surge: axisymmetric, periodic
- Rotating stall: progression around the blade annulus of a stall pattern, in which one or more adjacent blade passages are instantaneously stalled, then are cleared for unstalled flow as the stall cell progresses.
- Rotating stall causes alternate loading and unloading of the blades: fatigue failure.

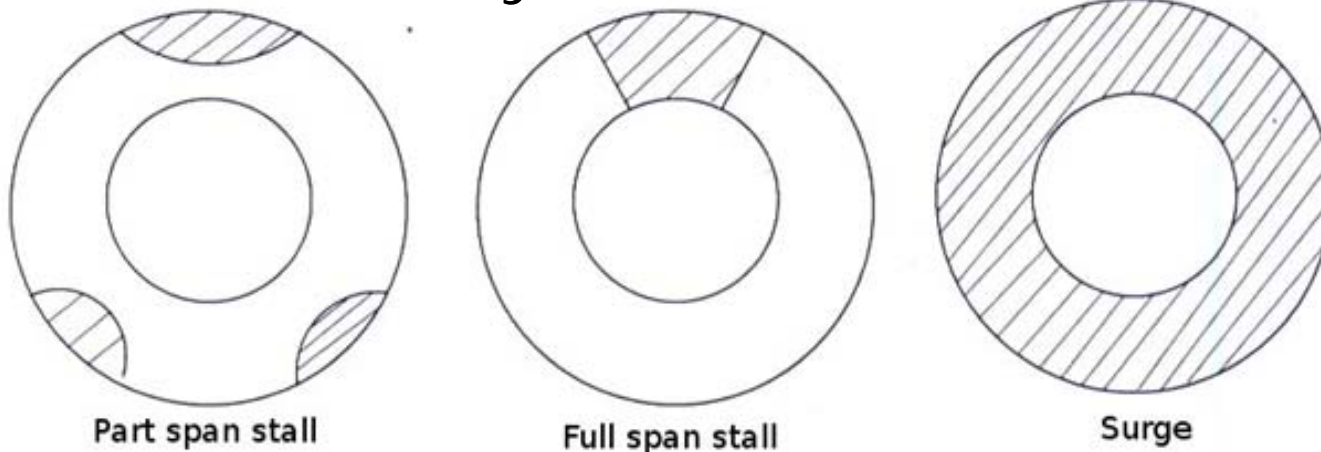
Multi-stage performance characteristics



Propagation of rotating stall

Multi-stage performance characteristics

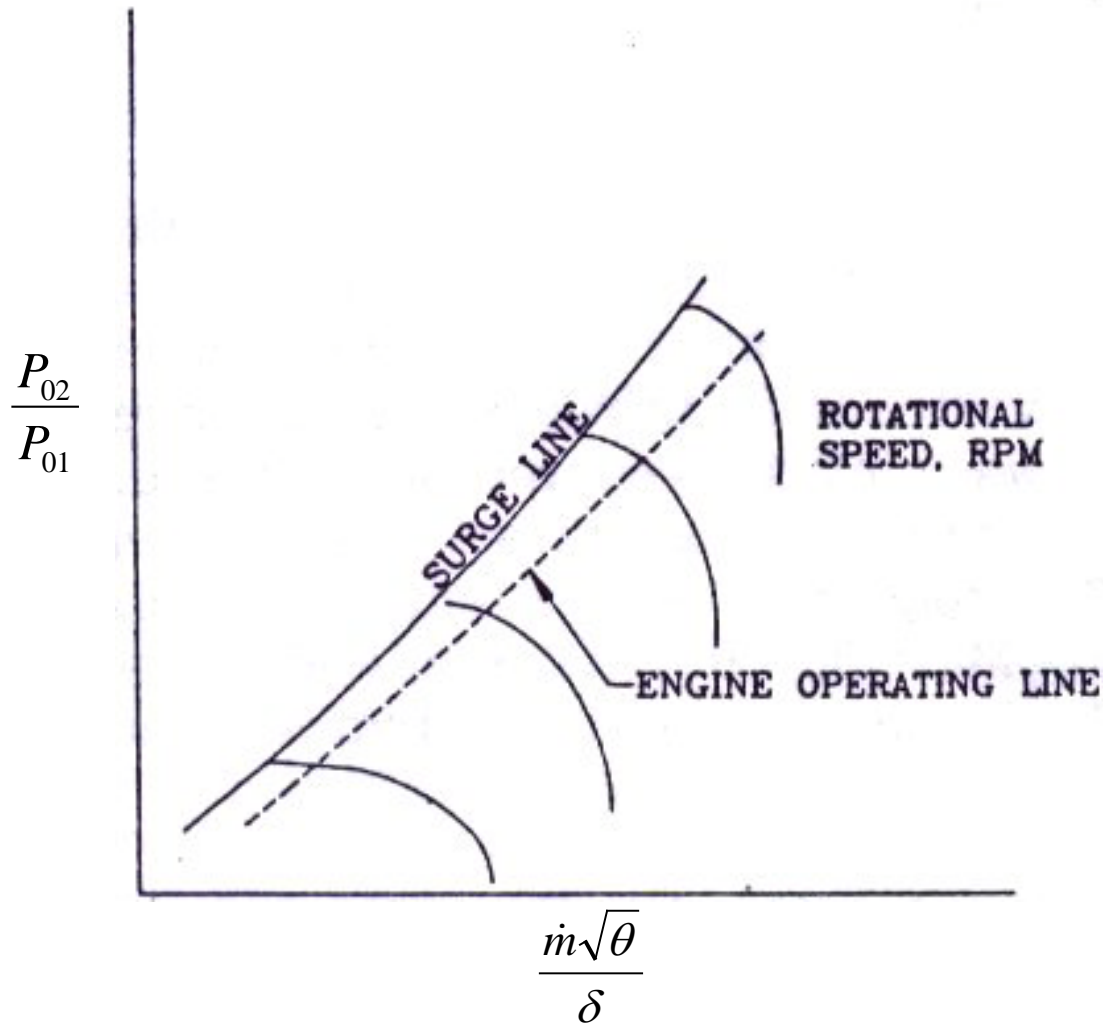
- Rotating stall often precedes surge.
- The stall patterns move in a direction opposite to that of the rotor revolution.
- The stall frequency can be as high as 50% of the rotor frequency.
- Rotating stall may be initiated by an incoming flow non-uniformity.



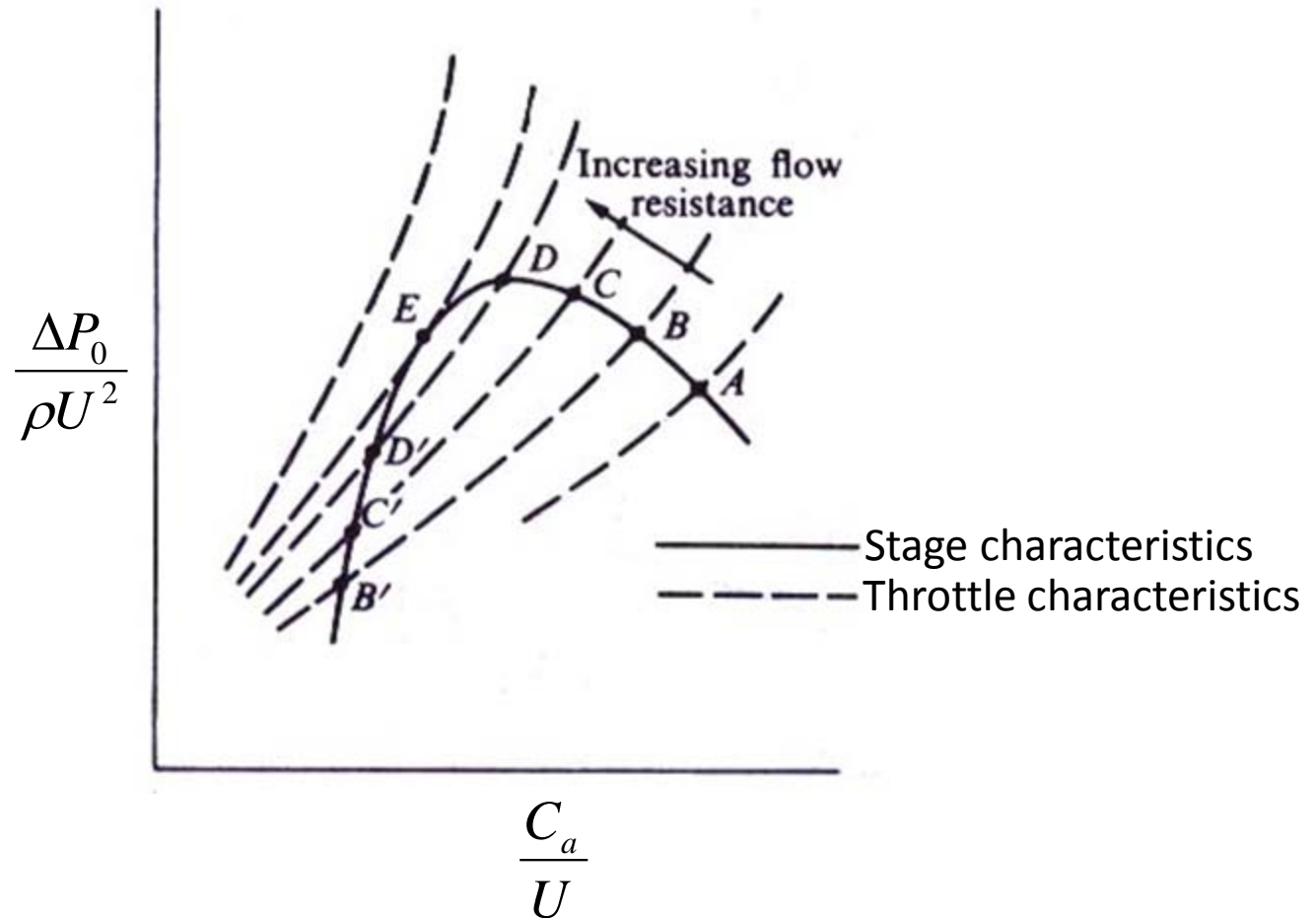
Multi-stage performance characteristics

- Surge line denotes the locus of unstable operation of the compressor.
- Surge is characterised by violent, periodic oscillations in the flow.
- Surge might lead to flame blow-out in the combustion chamber.
- Surge can lead to substantial damage to compressors and must be avoided.
- The operating line of the compressor is therefore kept slightly away from the surge line: **surge margin**.

Multi-stage performance characteristics



Multi-stage performance characteristics



In this lecture...

- Free vortex theory
- Single and multi-stage axial compressor characteristics

In the next lecture...

- Tutorial
 - Axial compressors